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June 23, 2023 12919

Tony Pauker VP Land Acquisition **Brookfield Properties** 733 8th Avenue San Diego, CA 92101

Subject: Otay Ranch Town Center Redevelopment Project Acoustical Assessment

Dear Mr. Pauker:

Dudek has completed this site-specific acoustical assessment for the Otay Ranch Town Center Redevelopment (TCR or "Project") located in the City of Chula Vista, California (City).

The project proposes a General Plan Amendment (GPA), Otay Ranch General Development Plan Amendment (Otay Ranch GDPA), Sectional Planning Area (SPA) Plan Amendment, and Planned Community (PC) Rezone. These amendments for FC-1 would allow development of 840 residential units (10% of which will be designated lowincome), while reducing the allowed commercial square footage from 960,000 square feet to 816,000 square feet. Development of the residential uses would be centered within the northwest portion of FC-1 and would have a density range of 18 to 56 units per acre. This area would have a new land use and zoning designation of Mixed-Use/Residential (MU/R). A total of three buildings are proposed; two residential buildings, and one mixeduse/residential building.

The proposed amendment would also change the name of the existing SPA from Freeway Commercial SPA to Otay Ranch Town Center SPA. In addition, the proposed amendment also includes 2.16 acres of public plaza/park space. The existing Town Center would continue to operate; however, demolition of 37,200 square feet of existing commercial space is proposed, and the addition of 146,000 square feet of new commercial uses would be constructed.

The purpose of this acoustical assessment is to support a fourth Addendum to the Final Environmental Impact Report for the Otay Ranch Freeway Commercial SPA Plan Planning Area 12 (FEIR), which already features noiserelated mitigation measures (reproduced for reader convenience) as follows:

- 5.5-1. Prior to the approval of site development plans, the Applicant shall submit a supplemental noise analysis acceptable to the Director of Planning and Building demonstrating:
  - Noise levels at the exterior use areas of the proposed hotels would not exceed 65 decibels (dBA) Community Noise Level Equivalent (CNEL).

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- Interior noise levels in habitable rooms of the proposed hotels would not exceed 45 dBA CNEL.
- Noise levels generated on the project site, being the combined noise levels of HVAC equipment, truck traffic, loading and unloading, and trash collection, where these may occur simultaneously, would not exceed the applicable limits of the noise ordinance.

In the context of the proposed project, this acoustical assessment presumes that the exterior use areas of proposed residential units would be subject to the same exterior noise threshold of 65 dBA CNEL; and, the inhabited interiors would need to comply with a background sound level (due to exterior-to-interior intrusion of traffic and other outdoor noise) of 45 dBA CNEL. Both of these standards are also consistent with City policies.

### 1 Introduction

#### 1.1 Acoustical Fundamentals

Although the terms may be used interchangeably in the right context, "sound" is defined as any gas or fluid pressure variation detected by the human ear, and "noise" is unwanted sound. The preferred unit for measuring sound is the decibel (dB), which by way of expressing the ratio of sound pressures to a reference value logarithmically enables a wide range of audible sound to be evaluated and discussed conveniently. On the low end of this range, zero dB is not the absence of sound energy, but instead corresponds approximately to the threshold of average healthy human hearing; and, on the upper end, 120–140 dB corresponds to an average person's threshold of pain.

The human ear is not equally responsive to all frequencies of the audible sound spectrum. An electronic filter is normally used when taking noise measurements that de-emphasizes certain frequencies in a manner that mimics the human ear's response to sound; this method is referred to as A-weighting. Sound levels expressed under the A-weighted system are sometimes designated dBA. All sound levels discussed in this report are A-weighted.

The equivalent continuous sound level ( $L_{eq}$ ) is a single dB value which, if held constant during the specified time period, would represent the same total acoustical energy of a fluctuating noise level over that same time period.  $L_{eq}$  values are commonly expressed for periods of one hour, but longer or shorter time periods may be specified.

The noise descriptor Community Noise Equivalent Level (CNEL) is typically used when describing community noise. CNEL energy-averages the varying sound levels occurring over a 24-hour period, but imparts a 10-decibel penalty to sound occurring between the hours of 10:00 p.m.–7:00 a.m. and a 5-dB penalty for noise between the hours of 7:00–10:00 p.m. as a means to account for increased noise sensitivity during nighttime and evening hours, respectively.

Additional common acoustical descriptors and terms that may assist the reader in framing the evaluation and discussion of noise in this report are provided in Appendix A.

Under controlled conditions in an acoustics laboratory, the trained, healthy human ear is able to discern changes in sound levels of 1 dBA when exposed to steady, single-frequency signals in the mid-frequency range. Outside such controlled conditions, the trained ear can detect changes of 2 dBA in normal environmental noise. It is widely

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accepted that the average healthy ear, however, can barely perceive noise level changes of 3 dBA. A change of 5 dBA is readily perceptible, and a change of 10 dBA is perceived as twice (if a gain) or half (if a loss) as loud. A doubling of sound energy results in a 3-dBA increase in sound, which means that a doubling of sound energy (e.g., doubling the volume of traffic on a road) would result in a barely perceptible change in sound level.

Sound propagation (i.e., the traverse of sound from a noise emission source position to a receiver location) is influenced by multiple factors that include geometric spreading, ground absorption, atmospheric effects, and occlusion by natural terrain and/or features of the built environment.

Sound levels attenuate (or diminish) geometrically at a rate of approximately 6 dBA per doubling of distance from an outdoor point-type source due to the spherical spreading of sound energy with increasing distance travelled. The effects of atmospheric conditions such as humidity, temperature, and wind gradients are typically distance-dependent and can also temporarily either increase or decrease sound levels measured or perceived at a receptor location. In general, the greater the distance the receiver is from the source of sound emission, the greater the potential for variation in sound levels at the receptor due to these atmospheric effects. Additional attenuation can result from sound path occlusion and diffraction due to intervention of natural (ridgelines, dense forests, etc.) and built features (such as solid walls, buildings and other structures).

#### 1.2 Vibration Fundamentals

Groundborne vibration is fluctuating or oscillatory motion transmitted through the ground mass (i.e., soils, clays, and rock strata). The strength of groundborne vibration attenuates rapidly over distance. Some soil types transmit vibration quite efficiently; other types (primarily sandy soils) do not. Several basic measurement units are commonly used to describe the intensity of ground vibration. The descriptors used by the Federal Transit Administration (FTA) are peak particle velocity (PPV), in units of inches per second (ips), and velocity decibel (VdB) that is based on a root-mean square (RMS) of the vibration signal magnitude. The calculation to determine PPV at a given distance is as follows:

$$PPV_{rcvr} = PPV_{ref}*(25/D)^n$$

#### Where:

 $PPV_{rcvr}$  is the peak particle velocity in inches per second of the equipment adjusted for distance (i.e., at the receiver);  $PPV_{ref}$  is the reference vibration level in inches per second at 25 feet; D = the distance from the equipment to the receiver; n is the Wiss exponent, for which a value of 1.5 would be consistent with FTA guidance. The above  $PPV_{rcvr}$  value can be converted to an RMS vibration velocity level as follows, where the crest factor (CF) is assumed to be a value of 4 per FTA guidance (FTA 2018):

$$VdB_{rcvr} = 20*LOG(PPV_{rcvr}/(CF*0.000001))$$

### 1.3 City of Chula Vista Standards

The City of Chula Vista General Plan Noise Element indicates that the maximum allowable exterior noise level for new residential developments is a Community Noise Equivalent Level (CNEL) of 65 A-weighted decibels (dBA) (City of Chula Vista 2005). Consistent with the California Building Code (CBC, Part 2, Title 24, California Code of Regulations) that stipulates "interior noise levels attributable to exterior sources shall not exceed 45 dB in any habitable room," the City of Chula Vista also requires that interior noise levels not exceed a CNEL of 45 dB within residences. Typically, with the windows open, building shells provide approximately 12-18 dB of noise reduction (OPR 2017). Therefore, rooms exposed to an exterior CNEL greater than 60 dB could result in an interior CNEL greater than 45 dB.

Section 19.68.030.A (Table III) of the City's Noise Ordinance sets exterior noise limits with respect to non-transportation sources from the Project as received by land use category type. For the multi-family residential buildings to the south of the Project, these limits are 60 dBA hourly  $L_{eq}$  during daytime hours (7:00 a.m. to 10:00 p.m.) and 50 dBA hourly  $L_{eq}$  during nighttime hours (10:00 p.m. to 7:00 a.m.).

## 2 Existing Conditions

### 2.1 Environmental Setting

FC-1 is 87.25 acres and is currently developed with commercial uses known as the Otay Ranch Town Center (Town Center). To date, 669,700 square feet of commercial area has been completed at the Town Center. Existing land uses at the Otay Ranch Town Center are primarily commercial in nature including retail, food and beverage, entertainment, and community-serving land uses (Figure 1 – Project Location).

## 2.2 Baseline Measurement Survey

An SPL measurement survey was conducted near the proposed project site on August 22, 2022, to quantify and characterize the representative existing outdoor ambient sound level. Table 3 provides the location, date, and time period at which these baseline noise level measurements were performed by an attending Dudek field investigator using a SoftdB-branded Model "Piccolo II" sound level meter (SLM) equipped with a 0.5 inch, pre-polarized condenser microphone with pre-amplifier. The SLM meets the current American National Standards Institute (ANSI) standard for a Type 2 sound level meter. The calibration status of the SLM was checked using a field calibrator before and after the measurements, and the measurements were conducted with the microphone positioned approximately 5 feet above the ground.

The SPL measurement locations are depicted as ST1, ST2, and ST3 in Figure 2 Baseline Noise Level Measurement Survey Locations. The measured L<sub>eq</sub>, L<sub>max</sub>, and L<sub>90</sub> noise levels are provided in Table 1. The primary observed and perceived noise sources during the approximate 15-minute SPL measurement consisted of intermittent roadway traffic along the nearby roadways (local streets and State Route 125 [SR125]), distant roadway and aviation traffic, distant conversations, and occasional dog barks, and birdsong. Beyond the summarized information presented in

Table 1, detailed noise measurement data and photographs of the survey locations are included in Appendix B, Baseline Noise Measurement Field Data.

Table 1. Measured Baseline Outdoor Ambient Noise Levels

Site	Location (Address)	Date (yyyy-mm-dd) and Start Time (hh:mm)	L <sub>eq</sub> (dBA)	L <sub>max</sub> (dBA)	L <sub>90</sub> (dBA)
ST1	Intersection of Wellbrook St. and Bedford Ave. (1585 Caminito Zaragosa)	2022-08-22 and 04:33 PM	56.9	82.3	49.6
ST2	Intersection of Impressionist Dr. and Canvas Dr. (1484 Canvas Drive)	2022-08-22 and 05:02PM	55.4	74.5	47.3
ST3	Near Town Center Dog Park, adjacent to SR125	2022-08-22 and 04:05 PM	60.9	71.0	55.3

Source: Appendix B.

**Notes**: Leq = equivalent continuous sound level (time-averaged sound level); Lmax = maximum sound level during the measurement interval; L90 = sound level exceeded 90% of the measurement interval; dBA = A-weighted decibels; ST = short-term noise measurement locations.

## 3 Methodology

## 3.1 Estimating Roadway Traffic Noise

The exterior noise analysis made use of the Federal Highway Administration (FHWA) Traffic Noise Model (TNM, version 2.5) (FHWA 2004) to predict future traffic noise exposure levels at multiple representative façade and balcony positions associated with the three-building project. Input data for the TNM modeling included the following: peak hour (PH) traffic volumes, vehicle speeds, and proportions of vehicle types. Peak hour traffic relied upon information displayed in Figure 5-2 and Figure 8-6 from the "Otay Ranch Town Center Reimagined Local Mobility Analysis" dated March 2<sup>nd</sup> (LLG 2022). Existing Traffic volumes for the SR125 freeway were based on the SANDAG Transportation Forecast Information Center Series ABM2+/2021 RP (SANDAG 2022).

Calculation of CNEL values from predicted hourly  $L_{eq}$  resulting from application of the TNM model using peak hour input data assumes the peak hour traffic volume is approximately equal to 10% of the average daily traffic (ADT). This relationship, based on typical traffic patterns, results in a CNEL value that is both comparable to the peak hour traffic  $L_{eq}$  estimate and representative of traffic noise resulting from typical daytime, evening and nighttime traffic distribution.

## 3.2 Estimating Construction Noise

Airborne construction noise and groundborne construction vibration are temporary phenomena, with emission levels varying from hour to hour and day to day, depending on the equipment in use, the operations performed, and

the distance between the source and receptor. Equipment that would be in use during construction would include, in part, an auger drill rig, man-lifts, excavators, backhoes, graders, loaders, cranes, flat-bed trucks, welders, pavers, rollers, and air compressors. The typical maximum noise levels at a distance of 50 feet from these various pieces of construction equipment and activities anticipated for use on the proposed project site are presented in Table 2. Note that the equipment noise levels presented in Table 2 are maximum noise levels. Usually, construction equipment operates in alternating cycles of full power and low power, producing average noise levels over time that are less than the maximum noise level. The average sound level of construction activity also depends on the amount of time that the equipment operates and the intensity of construction activities during that time.

**Table 2. Typical Construction Equipment Maximum Noise Levels** 

Equipment Type(s)	Maximum Noise Level (L <sub>max</sub> , dBA at 50 Feet)
Grader	85
Crane; Concrete Pump Truck; Excavator	81
Roller	80
Front End Loader	79
Backhoe; Compressor (air)	78
Paver	77
Man Lift	75
Flat Bed Truck	74
Welder / Torch	73

Source: FHWA 2006.

**Note:**  $L_{max}$  = maximum sound level; dBA = A-weighted decibels.

Aggregate noise emission from proposed project construction activities for each of the three anticipated buildings (MU/R-1, MU/R-2, MU/R-3), broken down by sequential phase, was predicted at an evaluation distance with respect to the nearest existing noise-sensitive receptor: the neighboring residence to the west of the proposed project. Because there are three anticipated buildings associated with the proposed project, this evaluation distance varies with the building (i.e., its construction site) geographic centroid position; hence, Table 3 presents a range of distance values with the smallest representing that of the closest proposed project mixed-use building.

Table 3. Estimated Distances between Construction Activities and the Noisesensitive Receptor Positions

Construction Phase	Equipment Type(s) Involved	Distance to Fixed Noise-Sensitive Receptor Position from Construction Site Centroid (Feet)
Demolition	concrete/industrial saws, rubber tired dozers, loaders, excavators	555 to 1,050
Site Preparation	rubber tired dozers, tractors/loaders/backhoes	510 to 920
Underground Utilities	tractors/loaders/backhoes	505 to 900

Table 3. Estimated Distances between Construction Activities and the Noisesensitive Receptor Positions

Construction Phase	Equipment Type(s) Involved	Distance to Fixed Noise-Sensitive Receptor Position from Construction Site Centroid (Feet)
Grading	excavators, graders, rubber tried dozers, tractors/loaders/backhoes	510 to 920
Building Construction	cranes, forklifts, generator sets, tractors/loaders/backhoes, welders	505 to 900
Paving	cement and mortar mixers, pavers, paving equipment, rollers, tractors/loaders/backhoes	460 to 870
Architectural Coating	air compressors	505 to 900

### 3.3 Estimating Construction Vibration

Section 1.2 provides the groundborne vibration propagation expression for estimating vibration velocity (in inches per second [ips] PPV) level at a receiving offsite structure. The typical vibration source amplitudes at a distance of 25 feet from the various pieces of construction equipment and activities anticipated for use on the proposed project site are presented in Table 4.

**Table 4. Vibration Source Amplitudes for Construction Equipment** 

Equipment Type(s)	Reference PPV at 25 ft. (in/sec)
Vibratory roller	0.210
Large bulldozer	0.089
Loaded trucks	0.076
Small bulldozer	0.003

**Source:** Caltrans 2020a Table 18. **Note:** PPV = Peak Particle Velocity.

## 3.4 Estimating Onsite Stationary Source Noise Propagation

Prediction of post-construction operation noise during nighttime hours attributed to operating onsite Project rooftop heating, ventilating, and air-conditioning (HVAC) equipment utilized Datakustik CadnaA that has algorithms based on the International Organization of Standardization (ISO) Standard 9613-2, "Attenuation of Sound During Propagation Outdoors, Part 2: General Method of Calculation" (ISO 1996). Source sound levels for the proposed Project and parameters utilized by the CadnaA outdoor sound propagation software are as follows:

- General Requirements B.1.b from the Master Precise Plan (Atlantis Group 2022) suggest proposed Project mechanical equipment would be located on building rooftops and "screened from view" with likely wells between or behind sloped gables or parapets; hence, the model assumes quantities of rooftop-mounted air-handling units (AHU), air-cooled chillers or condensing units (either termed "ACC" herein, meaning the outdoor-exposed components of air-conditioning systems), and ventilation fans (e.g., for the parking garages and commercial uses) are clustered within these visually bounded spaces and thus distributed across the roof of each building. While mechanical equipment schedules and roof plans showing locations of expected outdoor-exposed equipment for each building are not available at this time, a number of reasonable assumptions have been applied to estimate minimum outside air requirements, cooling load (i.e., refrigeration tonnage), and other parameters that in turn enable estimates of aggregate mechanical equipment noise emission from each mixed-used building. With more detail of the estimate calculations appearing in Appendix C, in summary these assumptions are as follows:
  - Each occupied 1,000 square feet of residential use is assumed to require 250 cubic feet per minute (CFM) of outside air (i.e., the introduction of "fresh" air for interior comfort); and, each 1,000 square feet of retail space is assumed to need 300 CFM (Loren Cook 1999).
  - Parking garages that may be wrapped by surrounding residential uses would be assumed to need mechanical ventilation on the order of 0.75 CFM per gross square foot (IMC 2015).
  - Residential units are assumed to require approximately one (1) ton of refrigeration per 400 square feet of inhabited space; and, retail (conservatively assumed to be restaurants or like uses) would need one ton per 125 square feet (Loren Cook 1999).

Although actual proposed project building design parameters may be different from these above assumptions, they are meant to conservatively help estimate the sound magnitudes of major noise-producing equipment and facilitate the assessment of onsite stationary-source operations to the neighboring offsite community.

- Acoustical ground absorption coefficient is estimated to be 0.50, which represents a blend of hard reflective surfaces (e.g., parking area pavement, rooftop surface) and absorptive ground cover (e.g., grassy landscaping and natural terrain).
- Acoustical reflection order is set at one (1), to account for one sound path reflection when contact is made with a modeled building surface.
- Climate conditions are 50 degrees Fahrenheit, 70% relative humidity.
- Although the topography of existing terrain surrounding the proposed project has been conservatively
  ignored for purposes of this acoustical assessment, the proposed project mixed-use buildings have all been
  rendered as four-story structures.

## 4 Compliance Criteria

In light of the applicable City general plan policies and noise ordinance regulations summarized in Section 1.3, this analysis uses the following standards to evaluate proposed project compliance and potential adverse effects to the surrounding community.

• Construction noise – although the City lacks construction noise limits, consistent with the FEIR this analysis applies a threshold of 70 dBA CNEL for temporary construction noise.

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- Onsite roadway traffic noise for purposes for this analysis, a direct roadway noise impact would be considered significant if predicted noise levels are greater than 65 dBA CNEL at receiving exterior uses of future residential units (e.g., balconies).
- Offsite roadway traffic noise would be considered significant if increases in roadway traffic noise levels attributed to the proposed project were greater than 3 dBA CNEL at an existing noise-sensitive land use.
- Off-site project-attributed stationary noise predicted noise exposure levels attributed to onsite proposed
  Project outdoor-exposed HVAC systems as received by neighboring community multi-family residential land
  uses at nighttime would need to be less than the City's standard of 50 dBA hourly Leq. The more stringent
  nighttime threshold of 50 dBA hourly Leq is applied rather than the daytime threshold of 60 dBA hourly Leq
  to assess impacts for continuous noise sources.
- Construction vibration although the County has no groundborne vibration limits specified in its Noise Ordinance, and the proposed project is considered exempt from building and zoning codes, for informational purposes this analysis applies guidance from Caltrans that indicates a vibration velocity level of 0.2 ips PPV received at a structure would be considered annoying by occupants within (Caltrans 2020). As for the receiving structure itself, aforementioned Caltrans guidance from Section 2.2 recommends that a vibration level of 0.3 ips PPV would represent the threshold for building damage risk to "older residential structures" such as those apparent on the offsite northern neighboring property.

## 5 Exterior Noise and Vibration Analysis Results

### 5.1 Off-Site Traffic Noise Exposure

The proposed project would result in the creation of additional vehicle trips on local arterial roadways (i.e., Town Center Drive and Olympic Parkway), which could result in increased traffic noise levels at adjacent noise-sensitive land uses. Appendix D, Traffic Noise Modeling Input and Output, contains a spreadsheet with traffic volume data (average daily traffic) for Town Center Drive and California Street, based on the Otay Ranch Town Center Reimagined Local Mobility Analysis (LLG 2022) and SANDAG Transportation Forecast Information Center Series ABM2+/2021 RP (SANDAG 2022) used for the proposed project. Potential noise effects from vehicular traffic were assessed using the Federal Highway Administration's Traffic Noise Model (TNM) version 2.5 (FHWA 2004). Information used in the model included the roadway geometry, posted traffic speeds, and traffic volumes for the following scenarios: existing (year 2020) and existing plus project.

The City's Noise Element establishes a policy for exterior sensitive areas to be protected from high noise levels. The Noise Element sets 65 dBA CNEL for the outdoor areas and 45 dBA CNEL for interior areas as the normally acceptable levels. For the purposes of this noise analysis, such impacts are considered significant when they cause an increase of 3 dB from existing noise levels. An increase or decrease in noise level of at least 3 dB is required before any noticeable change in community response would be expected (Caltrans 2013). According to acoustical principles, the increase in traffic noise level relates directly to the increase in volumes by the following expression:  $10*LOG(V_f/V_e)$ , where  $V_f$  is the future traffic volume,  $V_e$  is the existing traffic volume, and vehicle speeds and proportion of vehicle types are essentially unchanged. The project would have to roughly double the traffic volumes on local roadways to increase traffic by 3 dBA.

Traffic noise levels were also modeled at representative offsite noise-sensitive receivers ST1, ST2, and ST3 as shown in Figure 2. The receivers were modeled to be 5 feet above the local ground elevation. The noise model results are summarized in Table 5.

**Table 5. Roadway Traffic Noise Modeling Results** 

Modeled Receiver Tag	Existing (2020) Noise Level (dBA CNEL)	Existing (2020) Plus Project Noise Level (dBA CNEL)	Maximum Project-Related Noise Level Increase (dB)
ST1	68.2	68.2	< 0.1
ST2	68.8	68.8	< 0.1
ST3	60.9	60.9	< 0.1

Notes: dBA = A-weighted decibel; CNEL = Community Noise Equivalent Level; dB = decibel.

Table 4 shows that at all three listed representative receivers, the addition of proposed project traffic to the roadway network would result in a CNEL increase of less than 3 dB, which is below the discernible level of change for the average healthy human ear. Thus, a less-than-significant impact is expected for proposed project-related off-site traffic noise increases affecting existing residences in the vicinity.

### 5.2 Future Roadway Noise Exposures

Detailed site plan information provided by the Applicant was utilized to help properly depict roadway segments (i.e., Birch Road, Olympic Parkway, and Town Center Drive) and the exterior proposed Project facades, balconies, and patios. Representative consideration of proposed topography was also included in the traffic noise prediction model setup. For instance, the SR125 's grade sits approximately 15 feet below the grade of the project boundary. Figure 3 shows a plan view of the proposed Project tagged with callouts pointing to a large onsite open area and geographic locations of representative receivers along the street-facing facades of the planned three (3) Project buildings intended for residential occupation. Figure 4 displays an isometric view of the TNM model analysis space, showing all three (3) Project buildings and the proximity of the modeled roadway segments.

Table 6 presents the predicted exterior noise levels at the representative receptor locations appearing in Figures 3 and 4. Note that each of the three (3) residential building receptor locations includes four elevation positions that correspond with the building level or "floor" as identified in Table 6. Bold values are those that exceed 60 dBA CNEL, which would trigger the need for acoustical analysis as presented herein, and bold italicized values indicate predictions that exceed 65 dBA CNEL. Detailed input and output information from the TNM prediction model that supports these Table 6 values appear in Appendix D.

**Table 6. Predicted Exterior Noise Levels due to nearby Future Roadway Traffic** 

Duilding	Floor	Modeled	Modeled Receiver Location (see Figure 3)										
Building	FIOOI	1	2	3									
1	1st	54.3	59.8	N/A									
1	2nd	58.4	64.3	N/A									
1	3rd	60.0	65.0	N/A									

**Table 6. Predicted Exterior Noise Levels due to nearby Future Roadway Traffic** 

Duilding	Floor	Modeled F	Receiver Location (see	e Figure 3)
Building	Floor	1	2	3
1	4th	60.4	65.8	N/A
2	1st	51.3	N/A	N/A
2	2nd	55.6	N/A	N/A
2	3rd	57.7	N/A	N/A
2	4th	58.8	N/A	N/A
3	1st	40.4	51.6	51.9
3	2nd	44.2	55.5	54.9
3	3rd	46.1	59.5	56.9
3	4th	47.9	60.2	57.8
	) – 1 (Residential tyard)		35.8	

N/A = not available (position not modeled)

Predicted exterior sound levels presented in Table 5 that exceed 65 dBA CNEL proximate to a patio, balcony, or other usable outdoor space (e.g., open space) would need localized sound abatement to yield an outdoor level compliant with the City's 65 dBA CNEL standard. The prediction of traffic noise levels, with dominant acoustical contribution from the SR125 at Project buildout, as presented by the values in Table 6 is generally consistent with what would be expected from a high volume roadway at such distances, with exterior noise levels at the building facades increasing with floor height due to more direct traffic noise pathways to such receiver positions. The prediction of exterior noise levels at the western façade of Building MU/R-1 that exceed 65 dBA CNEL (due largely to exposure to SR125 traffic volumes and vehicle speeds) is also consistent with earlier traffic noise analyses from the EIR and previous Addenda. Consistent with Otay Ranch GDP policies, and as described in an earlier EIR Addendum, balconies planned on these residential units that are counted toward any open space requirements would incorporate appropriate sound attenuating project features around the perimeter of the balconies. An example means to provide this balcony sound abatement is presented in Section 7.1. As a result, these outdoor areas would not exceed the 65 dB CNEL threshold.

#### 5.3 Construction Noise Emission

A Microsoft Excel-based noise prediction model emulating and using reference data from the Federal Highway Administration Roadway Construction Noise Model (RCNM) was used to estimate construction noise levels at the nearest occupied noise-sensitive land use. (Although the RCNM was funded and promulgated by the Federal Highway Administration, it is often used for non-roadway projects, because the same types of construction equipment used for roadway projects are often used for other types of construction.) Input variables for the predictive modeling consist of the equipment type, the duty cycle for each piece of equipment (e.g., percentage of time within a specific time period, such as an hour, when the equipment is expected to operate at full power or capacity and thus make noise at a level comparable to what is presented in Table 2), and the distance from the noise-sensitive receiver. The predictive model also considers how many hours that equipment may be on site and operating (or idling) within an established work shift. Conservatively, no topographical features were assumed in the modeling. The RCNM has default duty-cycle values (i.e., acoustical usage factor [AUF]) for the various pieces of

equipment, which were derived from an extensive study of typical construction activity patterns. Those default duty-cycle values were used for this noise analysis, which is detailed in Appendix E, Construction Noise Modeling Input and Output, and produce the predicted results displayed in Table 7.

**Table 7. Predicted Construction Noise Levels per Activity Phase** 

Construction Phase	8-Hour L <sub>eq</sub> at Nearest Noise- Sensitive Receptor
Demolition	65.5
Site Preparation	63.2
Underground Utilities	59.9
Grading	64.7
Building Construction	61.3
Paving	62.5
Architectural Coating	51.5

Source: Appendix E.

Notes: L<sub>eq</sub> = equivalent noise level; dBA = A-weighted decibels.

As presented in Table 7, all proposed project construction activity noise levels would be less than the threshold of 70 dBA CNEL for temporary construction noise consistent with the FEIR, with most estimated to range between 60 and 65 dBA. However, under certain conditions construction noise may temporarily increase outdoor ambient levels above the daytime SPL measurements appearing in Table 1.

#### 5.4 Construction Vibration

Paving at the MU/R-1 building site would appear to occur as close as 450 feet to the eastern façade of the western residence across from SR125. The roller exhibits the highest vibratory magnitude amongst the equipment involved in paving activities. At this distance, and using a reference groundborne PPV of 0.21 ips for the roller at a distance of 25 feet, the estimated PPV at the receiving building façade can be estimated as follows:

$$PPV_{rcvr} = 0.21*(25/450)^{1.5} = 0.003 \text{ ips}$$
  
 $VdB_{rcvr} = 20*LOG(0.003/(4*0.000001)) = 57$ 

The predicted groundborne vibration velocity level is below the Caltrans guidance-based 0.3 ips PPV threshold for avoiding building damage to older residential structures.

For estimating potential building occupant annoyance, application of -3 VdB coupling loss on the above-estimated 57 VdB for the RMS signal would—by way of reverse-calculation of PPV from the reduced VdB—reduce the PPV as potentially perceived by building occupant to approximately 0.002 ips and thus less than the Caltrans-based guidance standard of 0.2 ips PPV for annoyance.

Subsequent onsite construction activities would involve greater quantities of equipment, but would be less vibratory than a roller and/or their distances would be much greater than this four hundred fifty-foot horizontal distance between the project site and the nearest residential building façade. Hence, groundborne vibration propagating from these more distance sources of onsite vibration would be substantially less than the preceding estimates for the roller and the Caltrans guidance-based vibration exposure thresholds.

### 5.5 Onsite Non-Transportation Noise Emission

The predicted aggregate hourly  $L_{eq}$  noise exposure from proposed Project onsite stationary sound sources is greater than 45.0 dBA but less than 50 dB at the two-nearest representative multi-family residential nearest sensitive receptors (i.e., ST1 and ST2, on the western side of ST125). Figure 5 displays these predicted operational sound levels visually across a horizontal plane on and beyond the proposed project site for the modeled nighttime scenario, which conservatively assumes residential and retail uses would be operating air-conditioning, ventilation, and refrigeration systems to keep building occupants (and refrigerated/frozen foods or other items) cool during hot summer months.

The more stringent nighttime threshold of 50 dBA hourly  $L_{eq}$  is applied rather than the daytime threshold of 60 dBA hourly  $L_{eq}$  to assess impacts for continuous noise sources. With the predicted noise exposure levels at nighttime being less than the City's standard of 50 dBA hourly  $L_{eq}$  for receiving multi-family residential land uses, Project onsite noise emission appears compliant and would not require implementation of special noise reduction measures.

## 6 Interior Noise Analysis

The prediction results from the preceding exterior noise analysis, provided in Table 5, indicate that future traffic noise levels at sample proposed project building facades would range close to but not exceed 66 dBA CNEL. With the 45 dBA CNEL interior background sound level limit, this means the minimum composite STC rating for the exterior shell separating the habitable interior space from the outdoor sound level should be at least 21. While this effective exterior-to-interior noise reduction value is greater than the aforementioned 12-17 dB range that can be expected from facades with open windows (OPR 2017), it is less than the 25-35 dB noise reduction range that FHWA guidance indicates can be achieved with closed storm windows on light-framed buildings or single-glazed closed windows on exterior masonry building walls (FHWA 2011). By way of example, a dual pane assembly composed of two 1/8"-thick glass panes separated by a 3/8" wide air-gap yields an STC rating of 31 (Viracon 2019). Because the City has adopted a thermal efficiency standard of a minimum U-factor of 0.58 (Chula Vista Municipal Code Sections 110.6, 150.0(q)), such dual-glazed window assemblies are expected and commonplace.

Hence, residential units with facades exposed to exterior noise levels greater than 65 dBA CNEL would be expected to have closed windows and balcony/patio doors in order to result in background sound levels that are compliant with the City's 45 dBA CNEL interior requirement (and be consistent with the California Building Code); thus, habitable spaces in such units would require mechanical means of ventilation and air-conditioning for interior comfort in order to keep such fenestration closed.

## 7 Recommendations

#### 7.1 Exterior Noise

As discussed in Section 5.1, residential units on the 4<sup>th</sup> floor (or above, depending on final design) of Building MU/R-1 directly facing SR125 highway traffic noise would have acoustically upgraded balconies in order to reduce outdoor noise exposure for seated occupants to 65 dBA CNEL or below. Consistent with the recommended sound abatement approach on previous Otay Ranch multi-family residential projects, one technique to provide this identified noise reduction need on the order of 5 dBA or less is the addition of a solid and sufficiently massive material layer to planned metal railings on the balcony usable area perimeter. As depicted in Figure 6, showing detail from a previously studied project (and thus used merely for illustration purposes), proposed installation of a 6-millimeter (0.236 inch) sheet of plexiglass (acrylic) on the interior-facing side of the balcony railing structure would be expected to yield an effective STC rating of at least 15. Although the material itself has an STC rating of 29 (Arkema Group 2019), the approximate 1"-wide air gap between the bottom edge of the plexiglass panel and the balcony floor results in lower expected STC performance. In other words, the area of the gap as a fraction of the barrier material surface area causes the reduction in sound transmission loss performance.

Other barrier material options and designs are possible, subject to non-acoustical considerations such as desired barrier opacity, balcony deck drainage, etc., provided that the designed installation has barrier material having adequate mass and solidity that yield a minimum net STC rating of 15 and an approximate deck to top-edge height of 42 inches (3.5 feet). For instance, the outdoor-exposed balconies requiring such sound abatement could incorporate solid, non-porous walls of comparable height (3.5') as part of their design.

Additionally, the final design of building MU/R-1 could relocate potentially affected western façade residential balconies studied herein to other facades where the outdoor noise exposures are predicted to be compliant with 65 dBA CNEL.

With respect to non-transportation noise emission from the proposed Project towards the surrounding community, Section 5.4 determined that predicted levels should be compliant with relevant City standards and thus not require any noise-reducing means or measures that are not already present in the current proposed design and layout of the Project features.

#### 7.2 Interior Noise

No special recommendations are needed with respect to providing an interior background sound level that is 45 dBA CNEL or less from the intrusion of future outdoor traffic noise. Customary closed dual-pane glazing on windows (and in the manufacture of balcony doors) as part of exterior building wall assemblies expected of modern building construction would provide anticipated and sufficient exterior-to-interior sound insulation to attain this City interior background noise threshold.

Dudek trusts that the results, findings, and recommendations presented in this letter report meet your needs for the proposed Project at this time. Should the City have comments on this report after its review, please let us know and we will address them at that time.

Sincerely,

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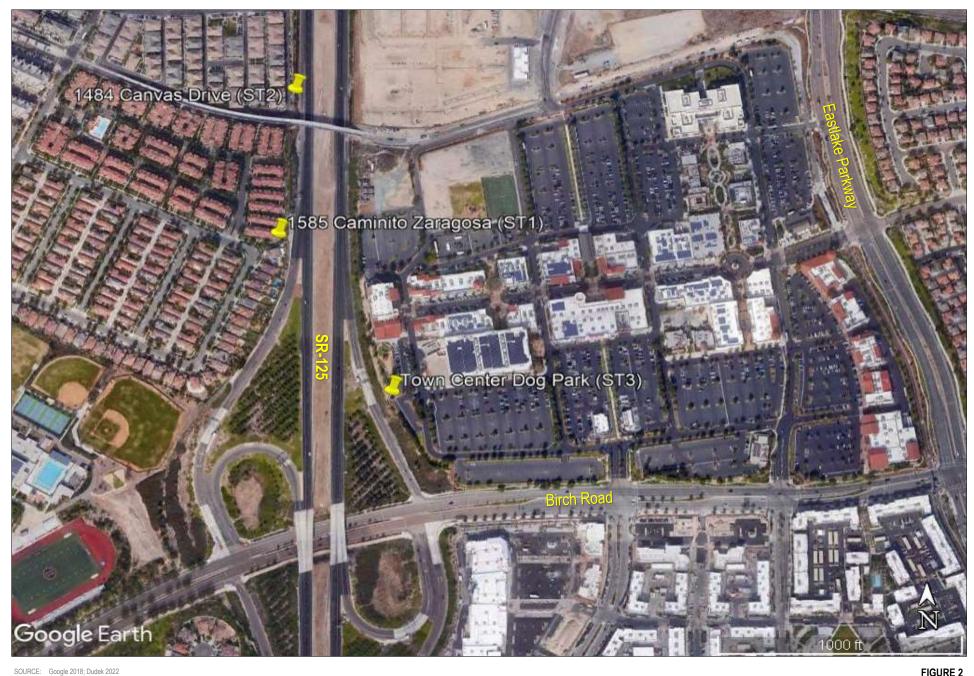
Viracon. 2019. http://www.viracon.com/pdf/ViraconAcousticPerfDataTables.pdf.



SOURCE: Bing Maps 2022

Project Location

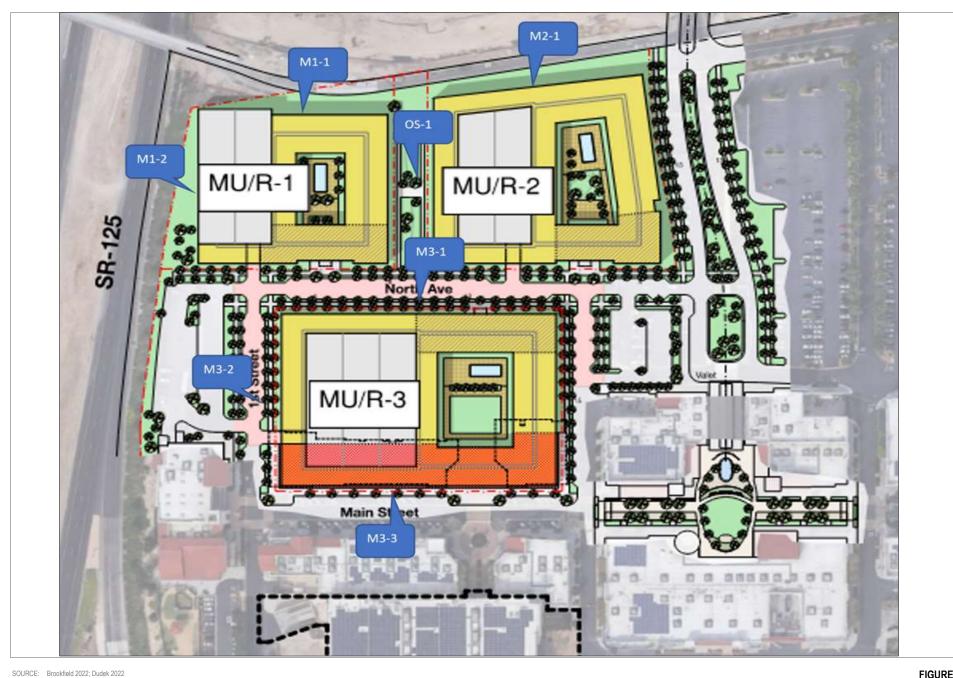
FIGURE 1

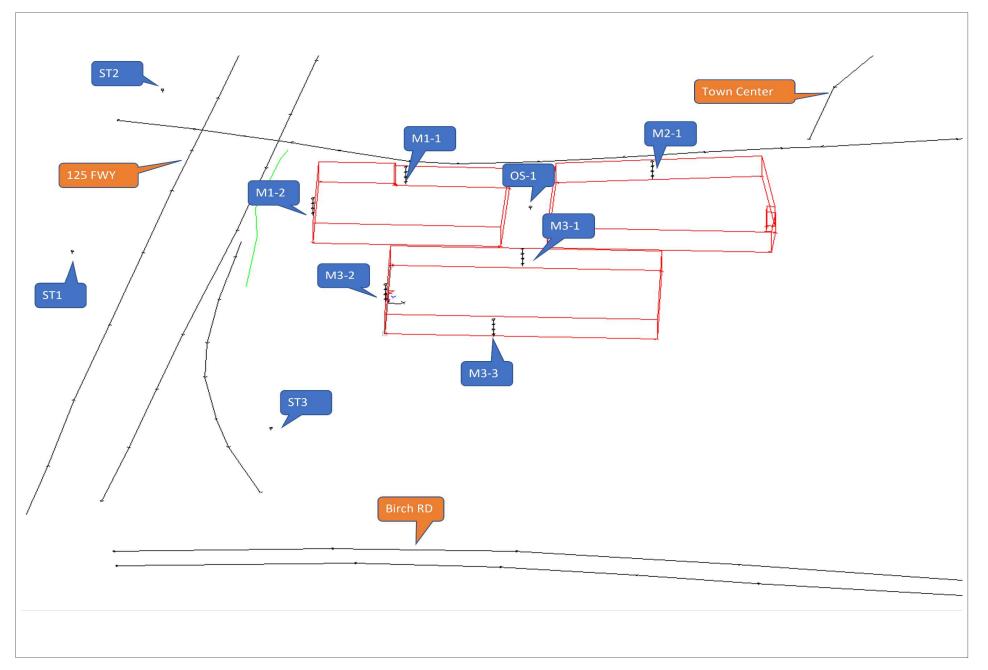


DUDEK &



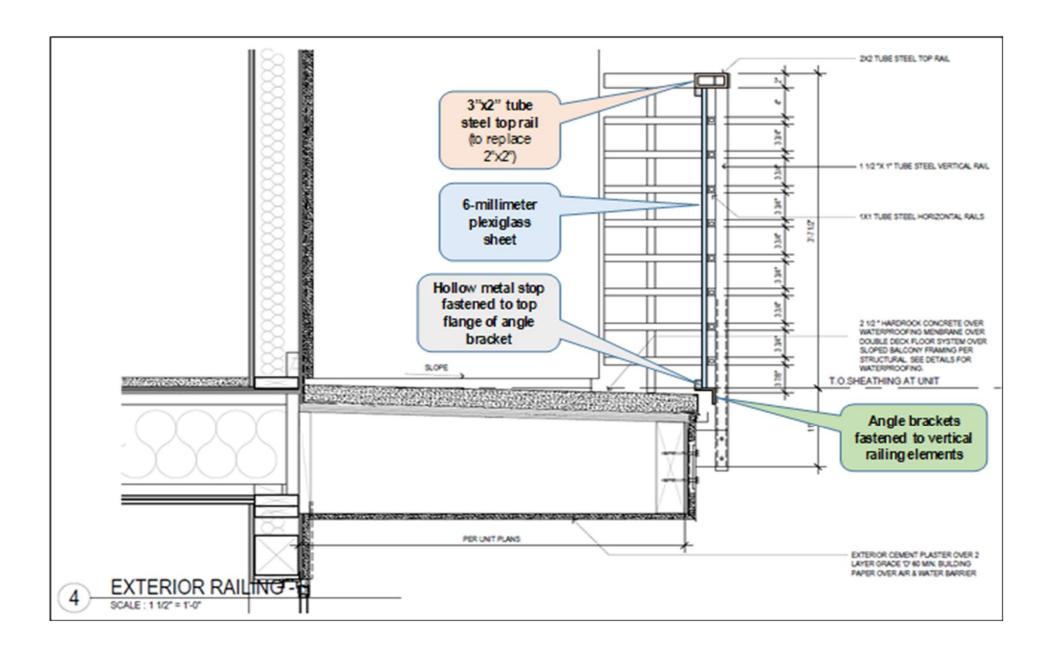
163.5 327 Feet













# Otay Ranch Town Center Redevelopment Project Acoustical Assessment

**Appendix A** – Glossary of Acoustical Terms

**Ambient Noise Level** 

The composite of noise from all sources near and far. The normal or existing level of environmental noise at a given location.

A-Weighted Sound Level (dBA)

The sound pressure level (SPL) in decibels as measured on a sound level meter (SLM) using the A-weighted filter network. The A-weighting filter de-emphasizes the very low and very high frequency components of the measured sound in a manner similar to the frequency response of the average healthy human ear, and thus correlates well with assessment of environmental noise in a community setting where noise-sensitive receptors may be present.

Decibel (dB)

The unit for expressing SPL and is equal to 10 times the logarithm (to the base 10) of the ratio of the measured sound pressure squared to a reference pressure, which is 20 micropascals.

Equivalent Sound Level (Leq)

The value corresponding to a steady-state sound level containing the same total energy as a time-varying signal over a given sample period.

Octave Band Center Frequency (OBCF)

Commonly discussed octave frequency bands are: 31.5 Hz, 63 Hz, 125 Hz, 250 Hz, 500 Hz, 1 kHz, 2 kHz, 4 kHz, 8 kHz and 16 kHz. Each of these "center frequencies" represents an octave band defined by a lower band limit equal to 0.707 times the center frequency, and an upper band limit equal to 1.414 times the center frequency.

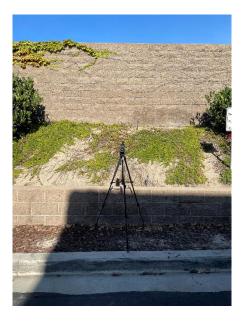
Sound Transmission Loss (TL)

The amount of sound, in decibels (dB), that is isolated by a material or partition in a particular OBCF or 1/3-OBCF. Example: 1/2" drywall has a TL at 125 Hz of 15 dB.1

Sound Transmission Class (STC)

A single-number rating that can be used to conveniently compare, acoustical isolation properties of different materials or assemblies. Generally, higher numbers indicate a material will provide more sound insulation when used as a barrier. Plotted against standardized STC curves, with established curve-fit tolerances, the TL of a material (in dB) at 500 Hz serves as the STC rating.

<sup>&</sup>lt;sup>1</sup> https://www.sweetwater.com/insync/sound-transmission-loss/









2103 - Looking east

2105 - Looking south

2106 - Looking north

2107 - Looking west



2095 - Looking east



2098 - Looking west



2090 - Looking northwest



2092 - Looking north



2093 - Looking northeast

Appendix B - Baseline Sound Level Survey Measurement Data

Numl	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022 8/22/2022	4:06:00 PM 4:07:00 PM 4:08:00 PM 4:08:00 PM 4:10:00 PM 4:11:00 PM 4:12:00 PM 4:13:00 PM 4:15:00 PM 4:16:00 PM 4:15:00 PM 4:19:00 PM 4:19:00 PM 4:19:00 PM 4:19:00 PM 4:19:00 PM 4:19:00 PM	4:06:00 PM 4:07:00 PM 4:08:00 PM 4:09:00 PM 4:10:00 PM 4:11:00 PM 4:12:00 PM 4:13:00 PM	0:01:00 At 0:01:00 At 0:01:00 At 1 0:01:00 A	uto Lovuto Lovut	w Minw Minw Minw Minw Minw Minw Minw Min	Slot   Slot	bow dow dow dow dow dow dow dow dow dow d	N% Freq \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	No N	16.44mV/P 78 16.44mV/P 76 16.44mV/P 76 16.44mV/P 76 16.44mV/P 76 16.44mV/P 88 16.44mV/P 75 16.44mV/P 79 16.44mV/P 76	3.1 72.8 3.6 72.8 3.8 73.3 3.7 73.8 76 72.8 3.8 73.2 3.9 72.1 3.3 74.5 70.7	60.4 59.7 59.1 61.8 60.9 61.5 61.7 62.2 59.9 59.5 62.5 59.7 60.6 61.1 61.1 60.2	82.3 83.2 84.4 85.8 88.3 83.3 81.1 81.3 84.8 87.3 93.9 82.5 81.9	79 63.1 79.7 62.2 79.9 61.1 80.8 66.8 80.4 7.8 81.9 68.8 79.9 66.8 81.6 65.5 76.7 67.7 75.2 64.7 79 67.1 89.3 65.3 89.3 65.3 77.1 66 66 78.7 67.7 75.6 66	68.5 70.4 68.3 71.4 68.5 70.1 68.3 71.5 69.3 69.2 71.1 67.9 66.9 69.3 69.3 69.3	65.9 67 65.2 67.7 66.3 66.4 65.9 68.3 66.5 65.9 66.3 67.4 65.9 65.6 65.7 65.7	ASmin LZI 55 53.8 53.7 55.3 52 50.5 54.1 53.1 53.9 52.8 53.6 51.5 52.5 54.7 53.3 57 57.2	95.3 96.4 96.6 94.5 93.8 94.6 94.7 98.1 93.2 92.8 92.3 97 95.4 99.8 93.4 93.3 94.4	90 90.6 91.1 91.6 90.6 91 89.9 92.3 89.3 88.5 88 91.4 90.6 94.5 89	77.5 76.9 79.6 78.7 79.3 78.1 79.3 79.5 80.7 77.3 80.3 77.5 78.4 78.9	ok LCp 100.1 98.9 99.7 96.3 97.3 96.9 100 101.7 97.9 93.3 94.1 99.3 97.6 94.9 94.7 98.4	93.6 93.4 89.8 90.8 93 94 98.1 90.6 89.2 94.3 93.6 104.7 93.7 88.7 94.5	86.3 81.4 76.7 80.1 82.4 78.5 79.5 79.7 83.4 85 80.2 81.6 84.4 82 79.3 78.2 80.7	63.5 63.6 62.5 62.6 61.6 61.6 66.5 66.5 70.5 65.6 65.9 65.9 65.6 67 66.8 65.9 64.4 64.8 66.8 65.9 65.2 65.2 65.7 66.7 66.8 65.8	2.3 64.65.65.65.65.66.66.65.68.65.63.9 67.5.65.66.65.68.63.9 67.5.65.66.66.66.66.66.66.66.66.66.66.66.6	9 62.7 2 61.9 4 61.3 5 64.5 5 63.1 9 65.1 7 63.9 5 64.6 6 65.9 5 62.2 9 62.7 2 65 1 63 3 64.4 4 64.7 4 63.2		61.9 61.2 60.4 63.3 61.6 63.1 61.1 62.4 63 64.1 61.1 60.6 63.3 60.2 61.1 60.2	59.5 60.3 58.9 60.6 57.4 60.5 59.7 61.4 60.5 59.8 58.6 61.6 59.8 58.6 61.6 59.8	55.1 55.1 57.6 52.5 53.7 54.9 55 57.6 54.1 54.8 51.9 57.4 55 56 54.8 55.8	54.1	99% 1/1 Oct. (dl 55.2 54 54 55.5 55.5 52 50.7 54.2 53.3 54.2 52.8 53.7 51.6 52.6 52.7 54.9 53.5 57.2 57.3	31.5 32.4 32.5 33.3 30 28.9 30.6 31.4 34.8 30 29 34 31.5 30.3 30.7 30.3 30.7 30.3	63 41.6 42.3 41.9 41.8 40.9 41.7 42.5 41 39.7 39.7 42 41.6 46.2 39.9 40.9 40.9 40.7	125 46.6 46.1 45.7 54.5 52.3 53.1 46.9 45.3 47.4 43.5 45.2 49.7 46.8 45.9 45.9 47.5	250 45.7 46.4 46.4 48.9 50.9 48.3 47.1 46.2 49.9 47.7 44.9 50.9 48.7 48.5 48.5 48.5 48.5 47.5 45.6	53.7 53	57 56.4 58.7 56.9 58.4 57.7 58.9 58.3 59.8 57.4 56.9 60 56.4 57.3 58.5 58.5	52.8 53.6 54.3	44.1 46.4 42.7 44.1 45.5 46.3 48 46.3 45.2 44.7 46.1 44.5 46	8000 36.3 33.7 33.8 35.6 32.2 32.9 35.6 35.4 37.6 35.6 34.5 34.5 35.6 34.5 35.6 36.8 39.7 36.8 39.7 36.2 33.3
	20 21 22 23 24 25 26 27 28 29 30 31 32 33 34	3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022 3/22/2022	4:34:00 PM 4:35:00 PM 4:36:00 PM 4:37:00 PM 4:38:00 PM 4:39:00 PM 4:40:00 PM 4:41:00 PM 4:42:00 PM 4:43:00 PM 4:44:00 PM 4:45:00 PM 4:45:00 PM 4:47:00 PM 4:47:00 PM	4:38:00 PM 4:39:00 PM 4:40:00 PM 4:41:00 PM 4:42:00 PM 4:43:00 PM 4:44:00 PM 4:45:00 PM 4:45:00 PM 4:47:00 PM	10 0:01:00 At 10 0:01:00 At 11 0:00 A	uto Lov	w Minw Minw Minw Minw Minw Minw Minw Min	Side   Side	bow dow dow dow dow dow dow dow dow dow d	BA No	No No No No No No No No No No No No No N	16.44mV/P 66 16.44mV/P 67 16.44mV/P 66 16.44mV/P 66 16.44mV/P 66 16.44mV/P 66	.4. 63.7 .5.5 63 .5.2 63.2 .6.6 65.4 .7.7 65.5 .7.5 68.5 .7.7 68.5 .7.7 63.5 .7.4 71.3 .0.6 66.2 .70 66.3 .72 64.4 .8.8 64.3 .9.9 63.5 .5.2 63.3 .6.6 63.3	51.3 52.4 50.7 51.8 51.4 52 52.5 50.5 67.2 52.4 52.2 52.4 52.5 50.6 50.6 50.6	71.8 68.9 73.1 72.2 74 88.5 72.7 72.3 89.3 75.4 76.7 72.8 72	71.4 63.5 68.4 5.6 68.7 53.1 68.8 54.2 70 55.1 68.8 68.3 62.2 71.4 54.4 84.1 82.2 73.3 61.4 72.1 53.3 65.4 69.4 69.1 69.2 69.1 53.6 68.2 53.3	65.5 62.4 63.3 62.6 62.7 62.4 63.6 61.6 61.9 62.5 64.3 64.3 64.5 64.5 64.5 64.5 64.5 64.5 64.5 64.5	60.7 60.6 60.3 60.4 60.3 61.1 59.1 59.3 59.8 61.7 61.1 62 60.2 59.9	50.5 49.1 49.6 49.1 49 48.3 48.6 48.9 49.2 49.4 48.9 49.4 48.8 49.2 48.6	83.3 84 86.4 85.5 85.3 90.5 85.8 83.5 91.8 87.4 87.8 85 84.6	80.8 81 83.2 83.3 82.3 86.3 82.3 81.3 89.1 84 84.1 82.2 82.1 81.3 81.1	69.2 69.8 70.7 70.3 68.3 85 70 70.2 69.8 71.2 68.6 68.4	78.5 83.4 83.8 87.6 84.4 86.1 107.8 86.4 82.7 108.1 89.3 89.4 84.3 83.8 87.4 83.8 86.3	81.1 79.1 81.2 81 81.8 101.4 85.4 80.7 101.8 83.8 84 82.5 82.5 80.1 79.7	70.6 66.2 66.9 70.5 69.9 92.2 86.6 67.6 97.8 80.3 70.3 79.6 77.2 66.8 67.1	62.2 60 54.6 5 81.5 79 60.3 59 57.9 57	3.7 53. 3.5 53. 3.1 53. 5.3 53. 5.4 54. 5.8 56. 5.8 56. 5.4 53. 9.2 75. 9.4 55. 7.7 56. 57 56. 58 59. 58 53.	3 53 1 52.2 7 53.4 9 53.1 6 54 8 55.6 7 55.9 1 52.4 6 68.8 4 54.6 1 54.7 2 55.5 6 56.3 3 52.6	52.7 52.9 51.9 53.3 52.8 53.5 54.3 51.9 64.2 54.1 54.3 54.3 55.3 52.4 52.9 51.4	52.6 52.6 52.1 52.6 52.1 52.5 52.3 51.2 50.7 53.7 51.7 52.6 51.9 51.5 51.4 51.1	52.3 52.4 50.4 51.6 51 50.9 50.5 49.9 50.7 51.8 50.7 51.8 50.2 50.2 49.7 49.6	51.5 49.6 49.9 49.6 49.6 49.1 49.3 49.3 49.5 49.9 49.6 49.7 49	50.9 49.4 49.8 49.5 49.3 49 48.8 49.1 49.3 49.7 49.2 49.6 48.9 49.3	51.7 50.7 49.2 49.6 49.3 49.4 48.7 48.9 49.2 49.4 49.4 49.4 49.4 48.8 49.2 49.2 48.7 48.9	23.6 21.9 22.6 24.1 24.1 23.5 28.8 24.6 21.2 28.5 25.1 26.3 23.4 23.7 23.3 23.3 24.9	32.6 32.9 33.1 35.9 37 38.1 34.2 34 36,4 36 35.7 34.3 33.9 33.2 33.2 33.5	37.6 38.7 38.7 41 41.4 39.8 37.1 41.6 38.6 43.2 40.2 40.2 38.5 37.1 36.6 37.3			49.3 46.9 47.5 47.6 46.7 47.5 47.7 46.6 64.9 49.2 47.9 47.9 48.9 47.3 47.2	44.8 43.2 43.6 43.8 43.2 46.2 46 42.8 48.4 44.4 43.6 43.8 43.3 43.7	38.4 36.8 36.7 36.8 36.4 45.1 44.9 36.5 45.6 37.2 36.9 37.5 37.5 36.6 36.9	30.4 30.3 28.9 29 28.9 29 36.5 36.8 28.7 38.6 29.7 28.9 30.1 28.8 28.6 28.7 29.2
	37	3/22/2022	4:51:00 PM	4:51:00 PM 4:52:00 PM 4:52:03 PM	1 0:01:00 Au	uto Lov	v Mi	s Slo	ow d	BA No BA No BA No	No	16.44mV/P 71 16.44mV/P 71	1.1 66.8 1.2 67.1 1.5 68.8	55.6 55.8 55.7 <b>55.8</b>	79.1	70.1 56 73.5 58.4 71.2 55.4 58.4	66.1 73	64.2 64.3 68.1	55.1 55.2 55.7 <b>55.2</b>		84.9	73.6	89.5 92.9 90.3		86.9	56 55 57.6 57 55.8 55		8 56.4		55.7 55.9 55.7	55.6 55.7 55.7	55.4	55.2 55.4 55.7		25.6	34.6 35.7 37.9	44.4	43.8	48.8		48.1		39.2 39.6 39.3
	40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58	3/22/2022 3/22/2022	5:01:36 PM 5:02:00 PM 5:03:00 PM 5:04:00 PM 5:05:00 PM 5:05:00 PM 5:05:00 PM 5:06:00 PM 5:10:00 PM 5:11:00 PM 5:11:00 PM 5:12:00 PM 5:14:00 PM 5:15:00 PM 5:15:00 PM 5:15:00 PM 5:16:00 PM 5:17:00 PM 5:17:00 PM 5:18:00 PM 5:18:00 PM	5:03:00 PM 5:04:00 PM 5:06:00 PM 5:06:00 PM 5:07:00 PM 5:09:00 PM 5:09:00 PM 5:11:00 PM 5:12:00 PM 5:14:00 PM 5:15:00 PM 5:16:00 PM 5:17:00 PM 5:19:00 PM 5:19:00 PM	0:01:00 At 0:01:00 At 0:01:00 At 1 0:01:00 A	uto Lovuto Lovut	W   Min   Mi	Slot   Slot	bow dow dow dow dow dow dow dow dow dow d	BA NO	No N	16.44mV/P 71 16.44mV/P 72 16.44mV/P 72 16.44mV/P 72 16.44mV/P 71 16.44mV/P 71 16.44mV/P 71 16.44mV/P 74 16.44mV/P 75 16.44mV/P 75 16.44mV/P 75 16.44mV/P 75 16.44mV/P 76 16.44mV/P 77 16.44mV/P 77 16.44mV/P 79 16.44	.9 67.2 .6 67.7 .3 71 .4 66.8 .8 65.2 .7 67.2 .3 67.3 .6 69.2 71 66.8 .9 69.6 .8 71.4 .8 66.1 .2 66.7 .8 66.1 .2 66.7 .8 68.8 .6 67.1 .2 64.8	60.9 52.5 53.2 61.9 51.3 52.9 51.9 54.7 53 55 54.7 52.6 61 55.3 52.2 54.9 53.3 52.9 54.9 53.3 55.4	79.6 77.9 85.2 82.6 80 76.5 81.9 76.1 83.8 77.7 80.3 86.4 81.7 87.5 76.8 76.7 79.4 78.7	72.8 66.73.7 58.9 61.78.9 61.1 74.2 57.3 74.2 58.3 60.4 59.3 76.6 68.3 75.9 63.7 75.9 75.9 75.9 75.9 75.9 75.9 75.9 75	63.8 64.7 64.7 61.8 60.9 63.5 64.1 62.5 65.9 62.4 62.8 65.5 62.3 66.7 65.1 66.7 65.1 66.7 65.1 66.7 65.1	61.1 61.9 59.4 62.1 59.2 59.3 58.3 60.9 60.7 60.2 60.8 59.9 64 62.6 59.8 59.9 62.6 60.9	49.1 45.7 47.3 44.9 48.1 43.4 44.8 45.4 46.5 45.7 46.8 44.2 49.7 42.7 42.7 42.1 45.6 42.1 49.7 42.0	89.7 90.4 90.1 89.2 86.6 89.5 88.1 92.4 88.8 91.7 91.1 93.6 87.6 87.6 88.4	85.3 85.5 88.8 84.6 83 85.1 87 84.6 87.4 86.4 89.2 88.7 83.9 84.5 86.6 84.9	70.3 71 70.8 79.7 69.1 70.7 69.7 71.9 70.8 72.8 72.5 70.4 78.8	86.6 92.9 92.9 98.2 95.3 94 89.7 96 88.6 93.4 95.3 101.8 93.3 87.8 91.5 92.2 84.4 90.4	85.3 88.6 93.8 95.5 90.5 85.9 89.3 83.6 91.3 93.1 93.1 93.9 91.9 94.3 86.4 86.3 86.5 86.7 82.7	78.1 79.7 77.5 93.5 82.3 71.2 74.6 72.7 78.8 73.7 73 83.3 77.5 76.4 72.5 70.8	57.5 57.8 57.8 57.8 55.5 54.5 58.7 58.6 60.2 65.1 64.6 60.4 60.4 60.4 60.6 68.6 67.6 68.6 67.6 63.	3.4 56.6 56.3.3 70.7 7.4 56.7 7.4 56.7 8.8 54.1 8.5 57.7 8.0 60 58.8 8.1.2 60.0 9.0 2 58.8 8.7 60.5 8.8 67.7 8.8 67.7 8.8 67.7 8.8 67.7 8.8 67.7 8.9 7.8 8.1 59.9 8.1 59.9	1 555 8 56.4 9 56.6 2 67 6 55.6 7 56.3 5 54.3 5 5 56.6 6 56.2 2 59.4 8 58.8 8 58.8 2 65.6 3 57.6 3 3 57.6 3 3 57.6 3 3 58.7 3 55.7 8 55.7 8 55.7 8		61.4 53.5 54.4 53.3 56.3 52.7 54.5 53.2 55.2 53.7 54.1 56.2 52.5 62.1 55.3 53.3 53.3 54.7 54.7 54.8	54.5 52 52.3 53.6 49.8 51.7 51.6 51.7 53.6 51.7 53.1 58.1 58.1 53.9 51.4 50.5 53.5 52.1 51.7	47.5 48.5 47.4 50.3 44.2 46.9 47.6 47.6 47.6 45.5 45.7 52.2 50.9 45.4 43.6 48.9 43.2 47.6	46.9 48 46.1 49.7 43.8 45.8 45.8 47.2 47.1 45.3 50.8 49.9 43.7 42.6 46.8 46.9	49.1 45.8 47.4 45.1 48.2 43.5 44.9 45.5 46.3 46.3 46.9 44.6 44.3 49.9 42.8 42.3 46 42.2 45.3 46	25.1 27.9 27.2 26.9 25.2 26.6 24.1 25.9 25.1 28.5 30.8 30.8 25 23.6 27.2 25.7 23.7 27		43.5 41.6	40.5	45.2 47	49.1 49.7 49.7 55.7 47.8 49.4 48.6 49.9 48.7 48.6 50.3 48.3 56.7 50.6 48.5 50.4 50.1 49.3	46.2 45.1 43.7 46.3 44.1 51.7 46.2 45.3 45.6 46.9 45.9	38 39.9 50.1 38.1 38.4 37.7 39.3 38 39.3 40.1 38.2 45.3 40.2 38.8 39.8 40.6 38.4 39.8	32.5 30.4 32.3 31.3 39 31.5 29.6 29.6 30.2 31.2 31.8 31.4 35.2 29.9 32.8 29.9 29.9 22.8 29.9 29.6

AHUs (plenum-type return fan only, no condenser units [see separate worksheet]):

):	A-weighting	adjustments	26	13	9	3	0	-1	-1	1
	average of values for the two fan diameter ranges, per Guyer (Table 12)	plug	40	40	38	34	29	23	19	16
	average of values for the two fan diameter ranges, per Guyer (Table 12)	tube	47	44	46	47	44	45	38	35
	per Guyer (Table 12, presumed based on Bies & Hansen ENC)	prop	46	48	55	53	52	48	43	38

												A-weighted PWL (for CadnaA inputs)										
Phase	Building Tag	GSF	Avg. SF/unit	Units	Adjusted Units	m²	facility function	CFM pksf *	m <sup>3</sup> /s per 1,000 m <sup>2</sup>		Q (m <sup>3</sup> /s)	fantype = plug, tube, or prop	63	125	250	500	1000	2000	4000	8000	OA dB	Q (cfm)
	s in building rooftop AHUs:	33.	711 gi 01 74 iii	- Cinto			identify runetion	or in pilot				tube, or prop	•	.20	200	000	1000	2000	1000	0000	O/ LUD	Q (0)
MU/R-1	residential units	230000	1150.0	200	200	21379	residence		250 1.27	625	27	plug	69	82	84	86	84	79	75	70	91	58000
MU/R-2	residential units	365000	1140.6	320	320	33927	residence		250 1.27	625	43	plug	71	84	86	88	86	81	77	72	93	92000
MU/R-3	residential units	365000	1140.6	320	320	33927	residence		250 1.27	625	43	plug	71	84	86	88	86	81	77	72	93	92000
MU/R-3	M	37200				3458	retail		300 1.52	626	5	plug	62	75	77	79	77	72	68	63	84	12000

\*source: Engineering Cookbook, 2nd ed., 1999 (Loren Cook Company)

ACCs (air-cooled chillers on rooftops):

	tons	PWL
Bryant BH16 018	1.5	67
Bryant BH16 024	2	71
Trane CGA 040	4	72
Trane CGA 080	8	74
Trane Flex 155Z	16	79
Trane Flex 1110Z	30	86
Daikin AGZ-E 60 (w/out sound insulation)	60	91
Daikin AGZ-E 120 (w/out sound insulation)	120	95
Daikin AGZ-E 240 (w/out sound insulation)	241	100

					Adjusted		Approx. Qty. of	tons per	Approx. Total		
Phase	Building Tag	GSF	Avg. SF/unit	Units	Units facility function	GSF per ton *	tons of refrig.	ACCs	ACC	PWL (dBA)	Notes
			_				-				
MU/R-1	residential units	230000	1150.0	200	200 apartment (high-rise), avg. of low and high	400	575.0	5	115	98	
MU/R-2	residential units	365000	1140.6	320	320 apartment (high-rise), avg. of low and high	400	912.5	7	130	103	
MU/R-3	residential units	365000	1140.6	320	320 apartment (high-rise), avg. of low and high	400	912.5	5	183	102	
	retail	37200	_		assume "restaurant" (avg. of hi and lo)	125	297.6	6	50	94	

\*source: Engineering Cookbook, 2nd ed., 1999 (Loren Cook Company)

Exhaus	st units (tubeaxial fans only):							A-wei	ghting adjustments	26	13	9	3	0	-1	-1	1	
					average of values for average of values for per Guyer (*	plug tube prop	40 47 46	40 44 48	38 46 55	34 47 53	29 44 52	23 45 48	19 38 43	16 35 38				
					0.75 = CFM per square foot of parking			fantype = plug,			A-weighted PWL							
Phase	Dullation Ton																	
	Building Tag	Parking Spaces	SF per pkg space	GSF	m <sup>*</sup> facility function	CFM	Pressure (Pa)	Q (m³/s)	tube, or prop	63	125	250	500	1000	2000	4000	8000	OA dB
	sting at above-bldg roof level (near ingress and egr		SF per pkg space	GSF	m <sup>c</sup> facility function	CFM	Pressure (Pa)	Q (m³/s)	tube, or prop	63	125	250	500	1000	2000	4000	8000	OA dB
				120000	m <sup>2</sup> facility function  11154 parking	<b>CFM</b> 90000 □	Pressure (Pa)	Q (m³/s)	tube, or prop	<b>63</b> 74	<b>125</b> 84	<b>250</b> 99	<b>500</b> 97	<b>1000</b> 97	<b>2000</b> 99	<b>4000</b> 92	<b>8000</b> 87	OA dB
fans exhau	sting at above-bldg roof level (near ingress and egr	ess)			, , , , , , ,	_		Q (m³/s) 42 68										

228000 'source: INTEC Controls, IMC 2015 Changes Affecting Parking Garage Exhaust SystemsImplementation, Revision 2.0, 2015, last accessed on May 26, 2018:http://inteccontrols.com/pdfs/IMC\_2015\_Changes\_for\_Parking\_Garages.pdf

INPUT: ROADWAYS		1			Otay Village Town Center									
Dudek					26 August 20	022								
CB					TNM 2.5	<i></i>								
INPUT: ROADWAYS							Average p	oavement typ	e shall be	used unles	S			
PROJECT/CONTRACT:	Otay Villa	age Town	Center			a State highway agency substantiates the use								
RUN:	Existing						of a differ	ent type with	the appro	val of FHW	A			
Roadway		Points												
Name	Width	Name	No.	Coordinates	(pavement)		Flow Con	trol		Segment				
				X	Y	Z	Control	Speed	Percent	Pvmt	On			
							Device	Constraint	Vehicles	Type	Struct?			
									Affected					
	ft			ft	ft	ft		mph	%					
125 South	55.0	point1	1	6,339,497.0	1,806,585.9	-15.00	)			Average				
		point2	2	6,339,495.5	1,806,799.0	-15.00	)			Average				
		point3	3	6,339,488.0	1,807,086.4	-15.00	)			Average				
		point4	4	6,339,490.0	1,807,415.0	-15.00				Average				
		point5	5	6,339,489.5	1,807,732.4	-15.00	)			Average				
		point6	6	6,339,490.0	1,808,004.1	-15.00	)			Average				
		point7	7	6,339,492.5	1,808,181.4	-15.00	)			Average				
		point8	8	6,339,495.5	1,808,410.0	-15.00	)			Average				
		point9	9	6,339,499.5										
125 North	55.0	•		6,339,629.5						Average				
		point11		6,339,627.0						Average				
		point12		6,339,625.5						Average				
		point13		6,339,626.0						Average				
		point14		6,339,625.5						Average				
		point15		6,339,616.0						Average				
		point16		6,339,614.5						Average				
		point17		6,339,612.5						Average				
Transit Dail	40.0	point18		6,339,609.0						A				
Transit Rail	12.0	•		6,341,131.0 6,340,975.5						Average				
		point20		6,340,975.5						Average				
		point21 point22		6,340,728.0						Average Average				
		point23		6,340,516.0						Average				
		point24		6,340,327.5						Average				
		point25		6,340,327.5						Average				

INPUT: ROADWAYS Otay Vil	llage Town Center
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III OII KOADIIAI O						otay vinago rown contor		
		point26	26	6,340,065.5 1,808,197.2	0.00		Average	
		point27	27	6,339,936.5 1,808,166.2	0.00		Average	
		point28	28	6,339,856.0 1,808,163.1	0.00		Average	
		point29	29	6,339,733.0 1,808,189.5	0.00		Average	
		point30	30	6,339,650.5 1,808,210.2	0.00		Average	Y
		point31	31	6,339,568.5 1,808,223.2	0.00		Average	Υ
		point32	32	6,339,482.5 1,808,238.0	0.00		Average	
		point33	33	6,339,351.5 1,808,254.2	0.00			
Town Center drive	12.0	point34	34	6,340,750.5 1,809,198.1	0.00		Average	
		point35	35	6,340,698.5 1,809,130.2	0.00		Average	
		point36	36	6,340,621.0 1,808,994.1	0.00		Average	
		point37	37	6,340,560.5 1,808,848.8	0.00		Average	
		point38	38	6,340,493.5 1,808,597.0	0.00		Average	
		point39	39	6,340,491.5 1,808,367.6	0.00		-	
Roadway5	45.0	point40	40	6,339,646.0 1,807,772.5	0.00		Average	
		point41	41	6,339,648.0 1,807,704.1	0.00		Average	
		point42	42	6,339,654.0 1,807,516.8	0.00		Average	
		point43	43	6,339,667.5 1,807,330.5	0.00		Average	
		point44	44	6,339,689.5 1,807,184.8	0.00		Average	
		point45	45	6,339,739.5 1,807,008.9	0.00		Average	
		point46	46	6,339,780.5 1,806,895.6	0.00		Average	
		point47	47	6,339,866.5 1,806,712.2	0.00			
Birch West	60.0	point48	48	6,342,049.0 1,806,628.9	0.00		Average	
		point49	49	6,341,718.5 1,806,557.0	0.00		Average	
		point50	50	6,341,498.5 1,806,534.4	0.00		Average	
		point51	51		0.00		Average	
		point52	52	6,340,691.5 1,806,547.0	0.00		Average	
		point53	53	6,340,320.5 1,806,539.1	0.00		Average	
		point54	54	6,340,020.5 1,806,498.2	0.00		Average	
		point55	55	6,339,668.0 1,806,423.4	0.00			
Birch east	60.0	point56	56	6,342,053.0 1,806,558.4	0.00		Average	
		point57	57	6,341,911.0 1,806,533.0	0.00		Average	
		point58	58	6,341,742.5 1,806,499.8	0.00		Average	
		point59	59	6,341,467.5 1,806,485.4	0.00		Average	
		point60	60	6,341,266.5 1,806,480.6	0.00		Average	
		point61	61	6,341,078.0 1,806,481.9	0.00		Average	
		point62	62	6,340,736.5 1,806,474.0	0.00		Average	
		point63	63		0.00		Average	
		point64	64	6,340,306.5 1,806,468.6	0.00		Average	

### INPUT: ROADWAYS Otay Village Town Center

		point65	5 6,340,068.5 1,806,443.5	0.00	Average
		point66	6 6,339,683.5 1,806,364.4	0.00	
Eastlake Pkwy	112.0	point67 6	7 6,341,641.5 1,808,823.6	0.00	Average
		point68 6	8 6,341,658.0 1,808,531.8	0.00	Average
		point69 6	9 6,341,674.0 1,808,284.4	0.00	Average
		point70 7	0 6,341,729.0 1,808,023.6	0.00	Average
		point71 7	1 6,341,794.0 1,807,792.6	0.00	Average
		point72 7	2 6,341,912.0 1,807,499.4	0.00	Average
		point73 7	3 6,341,988.0 1,807,319.1	0.00	Average
		point74 7	4 6,342,087.0 1,807,055.8	0.00	Average
		point75 7	5 6,342,125.0 1,806,860.6	0.00	Average
		point76 7	6 6,342,168.0 1,806,599.8	0.00	
Olympic west	60.0	point77 7	7 6,339,721.5 1,810,449.5	0.00	Average
		point78 7	8 6,339,934.5 1,810,298.0	0.00	Average
		point79 7	9 6,340,247.0 1,810,029.6	0.00	Average
		point80 8	0 6,340,524.0 1,809,614.9	0.00	Average
		point81 8	1 6,340,742.0 1,809,370.5	0.00	Average
		point82 8	2 6,340,941.0 1,809,234.1	0.00	Average
		point83	3 6,341,257.0 1,809,090.2	0.00	Average
		point84 8	4 6,341,595.0 1,808,969.2	0.00	
Olympic east	60.0	point85 8	5 6,341,594.5 1,808,888.2	0.00	Average
		point86 8	6 6,341,296.5 1,808,969.2	0.00	Average
		point87 8	7 6,341,120.0 1,809,026.4	0.00	Average
		point88 8	8 6,340,879.0 1,809,164.2	0.00	Average
		point89 8	9 6,340,645.0 1,809,369.5	0.00	Average
		point90 9	0 6,340,487.0 1,809,526.4	0.00	Average
		point91 9	1 6,340,376.0 1,809,672.0	0.00	Average
		•	2 6,340,286.0 1,809,816.9	0.00	Average
		point93	3 6,340,186.5 1,809,952.0	0.00	Average
		point94 9	4 6,340,076.0 1,810,076.4	0.00	Average
		<u>'</u>	5 6,339,967.0 1,810,185.8	0.00	Average
		point96	6 6,339,713.5 1,810,370.8	0.00	

ay Village Town isting pints ame No.		TNM 2	gust 2022 .5								
isting pints	Segme	TNM 2									
isting pints	Segme	ent .									
isting pints	Segme	ent									
isting pints	Segme	ent									
oints		ent									
		ent									
ame No.		nt									
	Autos										
			MTrucks	•	HTrucks	;	Buses		Motorcycles		
	V	S	V	S	V	S	V	S	V	S	
	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	
oint1	1 68	8 65	14	65	7	65	0	0	0	) (	
oint2	2 68	8 65	14	65	7	65	0	0	0	) (	
oint3	3 68	8 65	14	65	7	65	0	0	0	) (	
oint4	4 68	8 65	14	65	7	65	0	0	0	) (	
oint5	5 68	8 65	14	65	7	65	0	0	0	) (	
oint6	6 68	8 65	14	65	7	65	0	0	0	) (	
oint7	7 68	8 65	14	65	7	65	0	0	0	) (	
oint8	8 68	8 65	14	65	7	65	0	0	0	) (	
oint9	9										
oint10	10 58	65	12	65	6	65	0	0	0	) (	
oint11	11 58	2 65						0	0	) (	
oint12											
oint13								0	V veh/hr  0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		
oint14											
oint16											
oint17		65	12	65	6	65	0	0	0	) (	
oint18			_	_	_	_	_	_	_		
					_						
	pint11 pint12 pint13 pint14 pint15 pint16 pint17 pint18 pint19 pint20 pint21 pint22	bint11     11     58       bint12     12     58       bint13     13     58       bint14     14     58       bint15     15     58       bint16     16     58       bint17     17     58       bint18     18       bint19     19       bint20     20       bint21     21       bint22     22	bint11     11     582     65       bint12     12     582     65       bint13     13     582     65       bint14     14     582     65       bint15     15     582     65       bint16     16     582     65       bint17     17     582     65       bint18     18       bint19     19     0     0       bint20     20     0     0       bint21     21     0     0       bint22     22     0     0	bint11     11     582     65     12       bint12     12     582     65     12       bint13     13     582     65     12       bint14     14     582     65     12       bint15     15     582     65     12       bint16     16     582     65     12       bint17     17     582     65     12       bint18     18       bint19     19     0     0     0       bint20     20     0     0     0       bint21     21     0     0     0       bint22     22     0     0     0	bint11     11     582     65     12     65       bint12     12     582     65     12     65       bint13     13     582     65     12     65       bint14     14     582     65     12     65       bint15     15     582     65     12     65       bint16     16     582     65     12     65       bint17     17     582     65     12     65       bint18     18       bint19     19     0     0     0     0       bint20     20     0     0     0     0       bint21     21     0     0     0     0       bint22     22     0     0     0     0	bint11         11         582         65         12         65         6           bint12         12         582         65         12         65         6           bint13         13         582         65         12         65         6           bint14         14         582         65         12         65         6           bint15         15         582         65         12         65         6           bint16         16         582         65         12         65         6           bint17         17         582         65         12         65         6           bint18         18         65         12         65         6           bint19         19         0         0         0         0         0           bint20         20         0         0         0         0         0         0           bint21         21         0         0         0         0         0         0         0           bint22         22         0         0         0         0         0         0         0	bint11         11         582         65         12         65         6         65           bint12         12         582         65         12         65         6         65           bint13         13         582         65         12         65         6         65           bint14         14         582         65         12         65         6         65           bint15         15         582         65         12         65         6         65           bint16         16         582         65         12         65         6         65           bint17         17         582         65         12         65         6         65           bint18         18         65         6         65         65         65         65         65           bint20         20         0         0         0         0         0         0         0         0           bint21         21         0         0         0         0         0         0         0         0         0         0	bint11         11         582         65         12         65         6         65         0           bint12         12         582         65         12         65         6         65         0           bint13         13         582         65         12         65         6         65         0           bint14         14         582         65         12         65         6         65         0           bint15         15         582         65         12         65         6         65         0           bint16         16         582         65         12         65         6         65         0           bint17         17         582         65         12         65         6         65         0           bint18         18         0	bint11         11         582         65         12         65         6         65         0         0           bint12         12         582         65         12         65         6         65         0         0           bint13         13         582         65         12         65         6         65         0         0           bint14         14         582         65         12         65         6         65         0         0           bint15         15         582         65         12         65         6         65         0         0           bint16         16         582         65         12         65         6         65         0         0           bint17         17         582         65         12         65         6         65         0         0           bint18         18         8         8         6         6         6         6         6         6         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0	Dint11         11         582         65         12         65         6         65         0         0         0           Dint12         12         582         65         12         65         6         65         0         0         0           Dint13         13         582         65         12         65         6         65         0         0         0           Dint14         14         582         65         12         65         6         65         0         0         0           Dint15         15         582         65         12         65         6         65         0         0         0           Dint16         16         582         65         12         65         6         65         0         0         0           Dint17         17         582         65         12         65         6         65         0         0         0           Dint18         18         0         0         0         0         0         0         0         0         0         0         0           Dint20         20         0         0	

INPUT: TRAFFIC FOR LAeq1h Volumes		Otay Village Town Center										
	point24	24	0	0	0	0	0	0	0	0	0	0
	point25	25	0	0	0	0	0	0	0	0	0	0
	point26	26	0	0	0	0	0	0	0	0	0	0
	point27	27	0	0	0	0	0	0	0	0	0	0
	point28	28	0	0	0	0	0	0	0	0	0	0
	point29	29	0	0	0	0	0	0	0	0	0	0
	point30	30	0	0	0	0	0	0	0	0	0	0
	point31	31	0	0	0	0	0	0	0	0	0	0
	point32	32	0	0	0	0	0	0	0	0	0	0
	point33	33										
Town Center drive	point34	34	864	35	17	35	8	35	0	0	0	0
	point35	35	864	35	17	35	8	35	0	0	0	0
	point36	36	864	35	17	35	8	35	0	0	0	0
	point37	37	864	35	17	35	8	35	0	0		0
	point38	38	864	35	17	35	8	35	0	0	0	0
	point39	39										
Roadway5	point40	40	230	40	4	40	2	40	0	0	0	0
	point41	41	0	0	0	0	0	0	0	0	0	0
	point42	42	0	0	0	0	0	0	0	0	0	0
	point43	43	0	0	0	0	0	0	0	0	0	0
	point44	44	0	0	0	0	0	0	0	0	0	0
	point45	45	0	0	0	0	0	0	0	0	0	0
	point46	46	0	0	0	0	0	0	0	0	0	0
	point47	47										
Birch West	point48	48	1575	50	32	50	16	50	0	0	0	0
	point49	49	1575	50	32	50	16	50	0	0	0	0
	point50	50	1575	50	32	50	16	50	0	0	0	0
	point51	51	1575	50	32	50	16	50	0	0	0	0
	point52	52	1575	50	32	50	16	50	0	0	0	0
	point53	53	1575	50	32	50	16	50	0	0	0	0
	point54	54	1575	50	32	50	16	50	0	0	0	0
	point55	55										
Birch east	point56	56	1575	50	32	50	16	50	0	0	0	0
	point57	57	1575	50	32	50	16	50	0	0	0	0
	point58	58	1575	50	32	50	16	50	0	0	0	0
	point59	59	1575	50	32	50	16	50	0	0	0	0

INPUT: TRAFFIC FOR LAeq1h V	olumes of the state of the stat					Otay	Village	Town	Center			
	point60	60	1575	50	32	50	16	50	0	0	0	0
	point61	61	1575	50	32	50	16	50	0	0	0	0
	point62	62	1575	50	32	50	16	50	0	0	0	0
	point63	63	1575	50	32	50	16	50	0	0	0	0
	point64	64	1575	50	32	50	16	50	0	0	0	0
	point65	65	1575	50	32	50	16	50	0	0	0	0
	point66	66										
Eastlake Pkwy	point67	67	1626	50	33	50	16	50	0	0	0	0
	point68	68	1626	50	33	50	16	50	0	0	0	0
	point69	69	1626	50	33	50	16	50	0	0	0	0
	point70	70	1626	50	33	50	16	50	0	0	0	0
	point71	71	1626	50	33	50	16	50	0	0	0	0
	point72	72	1626	50	33	50	16	50	0	0	0	0
	point73	73	1626	50	33	50	16	50	0	0	0	0
	point74	74	1626	50	33	50	16	50	0	0	0	0
	point75	75	1626	50	33	50	16	50	0	0	0	0
	point76	76										
Olympic west	point77	77	1359	50	28	50	14	50	0	0	0	0
	point78	78	1359	50	28	50	14	50	0	0	0	0
	point79	79	1359	50	28	50	14	50	0	0	0	0
	point80	80	1359	50	28	50	14	50	0	0	0	0
	point81	81	1359	50	28	50	14	50	0	0	0	0
	point82	82	1359	50	28	50	14	50	0	0	0	0
	point83	83	1359	50	28	50	14	50	0	0	0	0
	point84	84										
Olympic east	point85	85	1359	50	28	50	14	50	0	0	0	0
	point86	86	1359	50	28	50	14	50	0	0	0	0
	point87	87	1359	50	28	50	14	50	0	0	0	0
	point88	88	1359	50	28	50	14	50	0	0	0	0
	point89	89	1359	50	28	50	14	50	0	0	0	0
	point90	90	1359	50	28	50	14	50	0	0	0	0
	point91	91	1359	50	28	50	14	50	0	0	0	0
	point92	92	1359	50	28	50	14	50	0	0	0	0
	point93	93	1359	50	28	50	14	50	0	0	0	0
	point94	94	1359	50	28	50	14	50	0	0	0	0
	point95	95	1359	50	28	50	14	50	0	0	0	0

INPUT: TRAFFIC FOR LAeq1h Volumes	Otay Village Town Center											
	point96	96										

INPUT: RECEIVERS					1	_		Otay Villag	je Town C	enter	
Dudek CB						26 Augus TNM 2.5	t 2022				
INPUT: RECEIVERS											
PROJECT/CONTRACT:	Otay \	/illage <sup>-</sup>	Town Center								
RUN:	Existi	ng									
Receiver											
Name	No.	#DUs	Coordinates	(ground)		Height	Input Sou	nd Levels	and Criter	ia	Active
			X	Y	Z	above	Existing	Impact C	riteria	NR	in
						Ground	LAeq1h	LAeq1h	Sub'l	Goal	Calc.
			ft	ft	ft	ft	dBA	dBA	dB	dB	
Town Center Dog Park	1	1	6,339,836.0	1,806,980.8	0.0	0 4.92	60.90	66	3 10.	0 8.	0 Y
ST1	2	1	6,339,381.0	1,807,674.9	0.0	0 4.92	56.90	66	6 10.	0 8.	0 Y
ST2	3	1	6,339,406.0	1,808,385.9	0.0	0 4.92	55.40	66	6 10.	0 8.	0 Y
M1-1	20	1	6,339,870.0	1,808,064.8	0.0	0 4.92	0.00	66	6 10.	0 8.	0 Y
M1-2	21	1	6,339,870.0	1,808,064.8	0.0	0 14.92	0.00	66	3 10.	0 8.	0 Y
M1-3	22	1	6,339,870.0	1,808,064.8	0.0	0 24.92	0.00	66	3 10.	0 8.	0 Y
M1-4	23	1	6,339,870.0	1,808,064.8	0.0	0 34.92	0.00	66	6 10.	0 8.	0 Y
M2-1	24		6,340,266.5	1,808,159.4	0.0	0 4.92	0.00	66	6 10.	0 8.	
M2-2	25		6,340,266.5	1,808,159.4	0.0	0 14.92	0.00	66	6 10.	0 8.	
M2-3	26		6,340,266.5	1,808,159.4	0.0	0 24.92	0.00			0 8.	
M2-4	27		0,0 .0,=00.0								
M3-1	28		-,,								
M3-2	30		0,0 10,1=110								
M3-3	31		-,,								
M3-4	33		0,0 10,1=110								
M4-1	34		-,,-		0.0						
M4-2	35		-,,-		0.0						
M4-3	36		-,,		0.0						
M4-4	37		-,,		0.0						
M5-1	38		-,,-		0.0						
M5-2	39		-,,-		0.0						
M5-3	40	1	6,339,925.5	1,807,559.1	0.0	0 24.92	0.00	66	6 10.	0 8.	0 Y

INPUT: RECEIVERS Otay Village Town Center

M5-4	41	1	6,339,925.5	1,807,559.1	0.00	34.92	0.00	66	10.0	8.0	Υ
M6-1	42	1	6,340,127.0	1,807,440.9	0.00	4.92	0.00	66	10.0	8.0	Υ
M6-2	43	1	6,340,127.0	1,807,440.9	0.00	14.92	0.00	66	10.0	8.0	Υ
M6-3	44	1	6,340,127.0	1,807,440.9	0.00	24.92	0.00	66	10.0	8.0	Υ
M6-4	46	1	6,340,127.0	1,807,440.9	0.00	34.92	0.00	66	10.0	8.0	Υ

Dudek					26 Augi	ust 2022												
СВ					TNM 2.5													
INPUT: BARRIERS																		
PROJECT/CONTRACT:		Village T	own Cer	iter														
RUN:	Existi	ng																
Barrier									Points									
Name	Type	Height		If Wall	If Berm	·	-	Add'tnl	Name	No.	Coordinates	(bottom)		Height	Segment			
		Min	Max	\$ per	\$ per	Тор	Run:Rise	\$ per			x	Υ	Z	at	Seg Ht Per	turbs	On	Importan
				Unit	Unit	Width		Unit						Point	Incre- #Up	#Dn	Struct?	Reflec-
				Area	Vol.			Length							ment			tions?
		ft	ft	\$/sq ft	\$/cu yd	ft	ft:ft	\$/ft			ft	ft	ft	ft	ft			
Barrier1	W	0.00	99.99	0.00				0.00	point1	1	6,339,727.0	1,808,050.1	0.00	40.00	0.00	0 (	)	
									point2	2	6,339,763.0	1,807,788.5	0.00	40.00	0.00	0 (	)	
									point3	3	6,340,071.5	1,807,828.0	0.00	40.00	0.00	0 (	)	
									point4	4	6,340,042.0	1,808,077.9	0.00	40.00	0.00	0 (	)	
									point5	5	6,339,852.5	1,808,057.1	0.00	40.00	0.00	0 (	)	
									point6	6	6,339,852.5	1,808,066.1	0.00	40.00	0.00	0 (	)	
									point7	7	6,339,727.0	1,808,050.1	0.00	40.00				
Barrier2	W	0.00	99.99	0.00				0.00	point8	8	6,340,147.5	1,807,836.6	0.00	40.00	0.00	0 (	)	
									point9	9	6,340,514.0	1,807,881.5	0.00	40.00	0.00	0 (	)	
									point10	10	6,340,506.5	1,807,966.0	0.00	40.00	0.00	0 (	)	
									point11	11	6,340,491.5	1,807,966.5	0.00	40.00	0.00	0 (	)	
									point12	12	6,340,487.5	1,807,990.9	0.00	40.00	0.00	0 (	)	
									point13	13	6,340,500.5	1,807,992.1	0.00	40.00	0.00	0 (	)	
									point14	14	6,340,442.5	1,808,201.2		40.00	0.00	0 (	)	
									point15	15		1,808,113.8				0 (	)	
									point16	16	6,340,147.5							
Barrier3	W	0.00	99.99	0.00				0.00	point17	17	-,,	1,807,715.4				0 (	)	
									point18	18	6,339,949.0	1,807,421.2	0.00	40.00	0.00	0 (	)	
									point19	19	-,,	1,807,476.6				0 (	)	
									point20	20	6,340,350.0	1,807,770.9	0.00	40.00	0.00	0 (	)	
									point21	21	6,339,906.5	1,807,715.4	0.00	40.00				

INPUT: TERRAIN LINES				
Dudek CB			26 August 20 TNM 2.5	22
INPUT: TERRAIN LINES				
PROJECT/CONTRACT: RUN:	Otay V Existin	illage Town C g	enter	
Terrain Line	Points			
Name	No.	Coordinates	(ground)	
		X	Y	Z
		ft	ft	ft
Terrain Line1	1	6,339,688.0	1,807,583.2	0.0
	2	6,339,667.5	1,807,799.5	0.0
	3	6,339,644.0	1,807,921.2	0.0
	4	6,339,647.5	1,808,134.1	0.0

5 6,339,654.0 1,808,178.0

0.00

		_				`	July Tilluge					1
Dudek							26 Augus	+ 2022				
CB							TNM 2.5	1 2022				
СВ							Calculate	d with TNI	M 2 E			
RESULTS: SOUND LEVELS							Calculate	u with Tin	WI 2.5			
PROJECT/CONTRACT:		Otov V	illaga Taum	Contor								
RUN:		Existin	illage Town	Center								
BARRIER DESIGN:			y HEIGHTS					Avorago	pavement type	s chall be use	d unloce	
DARRIER DESIGN.		INPUI	пеівпіз					_	ighway agenc			
ATMOSPHERICS:		68 deg	F, 50% RH						rent type with			
Receiver							<del>.</del>					
Name	No.	#DUs	Existing	No Barrier					With Barrier			
			LAeq1h	LAeq1h		Increase over	existing	Туре	Calculated	Noise Reduc	tion	
				Calculated	Crit'n	Calculated	Crit'n	Impact	LAeq1h	Calculated	Goal	Calculated
							Sub'l Inc	•	•			minus
												Goal
			dBA	dBA	dBA	dB	dB		dBA	dB	dB	dB
Town Center Dog Park	1	1	60.9	59.8	66	-1.1	10	)	59.8	0.0	8	-8.0
ST1	2	2	56.9	68.2	66	11.3	3 10	Both	68.2	0.0	8	-8.0
ST2	3	3	55.4	68.8	66	3 13.4	10	Both	68.8	0.0	8	-8.0
M1-1	20	) '	0.0	54.6	66	54.6	3 10		54.6	0.0	8	-8.0
M1-2	21	1 '	0.0	58.4	66	58.4	10		58.4	0.0	8	-8.0
M1-3	22	2	0.0	59.9	66	59.9	) 10		59.9	0.0	8	-8.0
M1-4	23	3	0.0	60.3	66	60.3	3 10		60.3	0.0	8	-8.0
M2-1	24	1 1	0.0	50.8	66	50.8	3 10		50.8	0.0	8	-8.0
M2-2	25	5 ′	0.0	55.1	66	55.1	10		55.1	0.0	8	-8.0
M2-3	26	6 1	0.0	57.2	: 66	57.2	2 10		57.2	0.0	8	-8.0
M2-4	27	7	0.0	57.6	66	57.6	3 10		57.6	0.0	8	-8.0
M3-1	28		0.0	40.4	- 66				40.4	0.0	8	-8.0
M3-2	30		0.0	44.1					44.1	0.0	8	
M3-3	31		0.0	46.1	66				46.1	0.0	8	
M3-4	33		0.0						47.8	0.0	8	-8.0
M4-1	34		0.0			58.3			58.3	0.0	8	
M4-2	35		0.0						63.6			
M4-3	36		0.0						65.0			
M4-4	37		0.0						65.8			
M5-1	38		0.0						51.6			
M5-2	39		0.0						55.4			
M5-3	40		0.0						59.5			
M5-4	41		0.0						60.2		1	
M6-1	42	2 1	0.0	51.6	66	51.6	3 10		51.6	0.0	8	-8.0

## **RESULTS: SOUND LEVELS**

43	1	0.0	5-	4.6	66	54.6	10		54.6	0.0	8	-8.0
44	1	0.0	5	3.6	66	56.6	10		56.6	0.0	8	-8.0
46	1	0.0	5	7.6	66	57.6	10		57.6	0.0	8	-8.0
	# DUs	Noise Red	duction									
		Min	Avg	N	/lax							
		dB	dB	d	IB							
	27	0.0	)	0.0	0.0							
	2	0.0	1	0.0	0.0							
	0	0.0	1	0.0	0.0							
	44	44 1 46 1 # DUs	# DUS Noise Remains dB 27 0.00 2 0.00	# DUS Noise Reduction Min Avg dB dB	# DUS Noise Reduction Min Avg dB dB c  27 0.0 0.0  2 0.0 0.0	44	44	44     1     0.0     56.6     66     56.6     10       46     1     0.0     57.6     66     57.6     10       # DUS     Noise Reduction       Min     Avg     Max       dB     dB     dB       27     0.0     0.0     0.0       2     0.0     0.0     0.0	44     1     0.0     56.6     66     56.6     10        46     1     0.0     57.6     66     57.6     10        # DUS     Noise Reduction       Min     Avg     Max       dB     dB     dB       27     0.0     0.0     0.0       2     0.0     0.0     0.0	44     1     0.0     56.6     66     56.6     10      56.6       46     1     0.0     57.6     66     57.6     10      57.6       # DUs Noise Reduction Min Avg Max       dB     dB     dB       27     0.0     0.0     0.0       2     0.0     0.0     0.0	44     1     0.0     56.6     66     56.6     10      56.6     0.0       46     1     0.0     57.6     66     57.6     10      57.6     0.0       # DUs Noise Reduction Min Avg dB     Max     Max       4B     dB     dB       27     0.0     0.0     0.0       2     0.0     0.0     0.0	44     1     0.0     56.6     66     56.6     10      56.6     0.0     8       46     1     0.0     57.6     66     57.6     10      57.6     0.0     8       # DUs Noise Reduction Min Avg dB     Max       dB     dB     dB       27     0.0     0.0     0.0       2     0.0     0.0     0.0

NFOI. NOADWAIG	T					1	Otay	Village TOWIT	Ocinioi		
Dudek					26 August 20	022					
CB					TNM 2.5	<b>-</b>					
INPUT: ROADWAYS							Δverage	pavement typ	e shall be	usad unlas	<b>C</b> :
PROJECT/CONTRACT:	Otay Villa	nga Town	Center					ighway agend			
RUN:	Existing		Ocinici					rent type with			
	Exioning	Points						Tone typo with			
Roadway	Width		Na	Coordinates	(navamant)		Flow Co	ntual		Cammant	
Name	widin	Name	No.	Coordinates	1	-	Flow Co	and the second s	D	Segment	0
				X	Y	Z	Control	Speed	Percent	Pvmt	On Ctrust2
							Device	Constraint	Vehicles	Туре	Struct?
	ft			ft	ft	ft		mnh	Affected %		
								mph	70		
125 South	55.0	•		6,339,497.0						Average	
		point2		6,339,495.5						Average	
		point3		6,339,488.0						Average	
		point4		6,339,490.0						Average	
		point5		6,339,489.5						Average	
		point6		6,339,490.0						Average	
		point7		6,339,492.5						Average	
		point8		6,339,495.5						Average	
		point9		6,339,499.5							
125 North	55.0	point10		6,339,629.5						Average	
		point11	11							Average	
		point12		6,339,625.5						Average	
		point13		6,339,626.0	1,808,123.2					Average	
		point14		6,339,625.5						Average	
		point15		6,339,616.0						Average	
		point16		6,339,614.5						Average	
		point17	17	· · · · · · · · · · · · · · · · · · ·						Average	
		point18		6,339,609.0							
Transit Rail	12.0	•		6,341,131.0						Average	
		point20	20	- , ,						Average	
		point21	21	<u> </u>						Average	
		point22		6,340,516.0						Average	
		point23		6,340,449.5						Average	
		point24		6,340,327.5						Average	
		point25	25	6,340,201.5	1,808,241.9	0.00				Average	

INPUT: ROADWAYS	Otay Village Town Center
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III O II NOADIIAI O				Olay Village	, iouii ooiitoi	
		point26	26 6,340,065.5 1,808,197.2	0.00	Average	)
		point27	27 6,339,936.5 1,808,166.2	0.00	Average	)
		point28	28 6,339,856.0 1,808,163.1	0.00	Average	÷
		point29	29 6,339,733.0 1,808,189.5	0.00	Average	<b>&gt;</b>
		point30	30 6,339,650.5 1,808,210.2	0.00	Average	e Y
		point31	31 6,339,568.5 1,808,223.2	0.00	Average	e Y
		point32	32 6,339,482.5 1,808,238.0	0.00	Average	<b>.</b>
		point33	33 6,339,351.5 1,808,254.2	0.00		
Town Center drive	12.0	point34	34 6,340,750.5 1,809,198.1	0.00	Average	<b>.</b>
		-	35 6,340,698.5 1,809,130.2	0.00	Average	
		point36	36 6,340,621.0 1,808,994.1	0.00	Average	<u> </u>
			37 6,340,560.5 1,808,848.8	0.00	Average	
			38 6,340,493.5 1,808,597.0	0.00	Average	
			39 6,340,491.5 1,808,367.6	0.00		
Roadway5	45.0	-	40 6,339,646.0 1,807,772.5	0.00	Average	<u> </u>
·		-	41 6,339,648.0 1,807,704.1	0.00	Average	
		•	42 6,339,654.0 1,807,516.8	0.00	Average	
		•	43 6,339,667.5 1,807,330.5	0.00	Average	
		· ·	44 6,339,689.5 1,807,184.8	0.00	Average	
		=	45 6,339,739.5 1,807,008.9	0.00	Average	
		-	46 6,339,780.5 1,806,895.6	0.00	Average	
			47 6,339,866.5 1,806,712.2	0.00		
Birch West	60.0	•	48 6,342,049.0 1,806,628.9	0.00	Average	<b></b>
		· ·	49 6,341,718.5 1,806,557.0	0.00	Average	
		-	50 6,341,498.5 1,806,534.4	0.00	Average	
			51 6,341,239.5 1,806,545.9	0.00	Average	
		•	52 6,340,691.5 1,806,547.0	0.00	Average	
		•	53 6,340,320.5 1,806,539.1	0.00	Average	
		· ·	54 6,340,020.5 1,806,498.2	0.00	Average	
		-	55 6,339,668.0 1,806,423.4	0.00		
Birch east	60.0	•	56 6,342,053.0 1,806,558.4	0.00	Average	خـ
		•	57 6,341,911.0 1,806,533.0	0.00	Average	
		-	58 6,341,742.5 1,806,499.8	0.00	Average	
		•	59 6,341,467.5 1,806,485.4	0.00	Average	
		-	60 6,341,266.5 1,806,480.6	0.00	Average	
		-	61 6,341,078.0 1,806,481.9	0.00	Average	
		טטווונט ו				
		•				
		point62	62 6,340,736.5 1,806,474.0 63 6,340,533.0 1,806,473.2	0.00	Average Average	Э

## **INPUT: ROADWAYS**

		point65	65 6,340,068.5 1,806,443.5	0.00	Average
		point66	66 6,339,683.5 1,806,364.4	0.00	
Eastlake Pkwy	112.0	point67	67 6,341,641.5 1,808,823.6	0.00	Average
		point68	68 6,341,658.0 1,808,531.8	0.00	Average
		point69	69 6,341,674.0 1,808,284.4	0.00	Average
		point70	70 6,341,729.0 1,808,023.6	0.00	Average
		point71	71 6,341,794.0 1,807,792.6	0.00	Average
		point72	72 6,341,912.0 1,807,499.4	0.00	Average
		point73	73 6,341,988.0 1,807,319.1	0.00	Average
		point74	74 6,342,087.0 1,807,055.8	0.00	Average
		point75	75 6,342,125.0 1,806,860.6	0.00	Average
		point76	76 6,342,168.0 1,806,599.8	0.00	
Olympic west	60.0	point77	77 6,339,721.5 1,810,449.5	0.00	Average
		point78	78 6,339,934.5 1,810,298.0	0.00	Average
		point79	79 6,340,247.0 1,810,029.6	0.00	Average
		point80	80 6,340,524.0 1,809,614.9	0.00	Average
		point81	81 6,340,742.0 1,809,370.5	0.00	Average
		point82	82 6,340,941.0 1,809,234.1	0.00	Average
		point83	83 6,341,257.0 1,809,090.2	0.00	Average
		point84	84 6,341,595.0 1,808,969.2	0.00	
Olympic east	60.0	point85	85 6,341,594.5 1,808,888.2	0.00	Average
		point86	86 6,341,296.5 1,808,969.2	0.00	Average
		point87	87 6,341,120.0 1,809,026.4	0.00	Average
		point88	88 6,340,879.0 1,809,164.2	0.00	Average
		point89	89 6,340,645.0 1,809,369.5	0.00	Average
		point90	90 6,340,487.0 1,809,526.4	0.00	Average
		point91	91 6,340,376.0 1,809,672.0	0.00	Average
		point92	92 6,340,286.0 1,809,816.9	0.00	Average
		point93	93 6,340,186.5 1,809,952.0	0.00	Average
		point94	94 6,340,076.0 1,810,076.4	0.00	Average
		point95	95 6,339,967.0 1,810,185.8	0.00	Average
		point96	96 6,339,713.5 1,810,370.8	0.00	

Dudek				26 Aug	just 2022	•						
CB				TNM 2	•	•						
СБ				I INIVI Z	.5							
INPUT: TRAFFIC FOR LAeg1h Volumes												
PROJECT/CONTRACT:	Otay Village	Town Co	enter									
RUN:	Existing + P		J.1101									
Roadway	Points	, ,										
Name	Name	No.	Segmen	  f								
			Autos		MTrucks	 	HTrucks	 	Buses		Motorcy	/cles
			V	s	V	s	V	s	V	s	V	s
			veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph
125 South	point1	1				<u> </u>				<u> </u>		
.20 33411	point2	2										
	point3	3									0	
	point4	4		65	14	65	7	65	C	C	0	C
	point5	5	688	65	14	65	7	65	C	) C	0	) (
	point6	6	688	65	14	65	7	65	C	0	0	0
	point7	7	688	65	14	65	7	65	C	) c	0	
	point8	8	688	65	14	65	7	65	0	C	0	0
	point9	9										
125 North	point10	10	582	65	12	65	6	65	C	C	0	C
	point11	11	582	65	12	65	6	65	0	) c	0	
	point12	12	582	65	12	65	6	65	0	C	0	
	point13	13	582	65	12	65	6			C	0	0
	point14	14							_	) C	0	) c
	point15	15		65						C	0	
	point16	16		65								0
	point17	17		65	12	65	6	65	C	C	0	C
	point18	18										
Transit Rail	point19	19					_				_	
	point20	20					-				_	
	point21	21										
	point22	22		0	0							
	point23	23	0	0	0	0	0	0	0	) C	0	

NPUT: TRAFFIC FOR LAeq1h Vol	lumes					Ota	ay Villag	e Town	Center			
•	point24	24	0	0	0					0	0	(
	point25	25	0	0	0	0	0	0	0	0	0	(
	point26	26	0	0	0	0	0	0	0	0	0	(
	point27	27	0	0	0	0	0	0	0	0	0	(
	point28	28	0	0	0	0	0	0	0	0	0	(
	point29	29	0	0	0	0	0	0	0	0	0	(
	point30	30	0	0	0	0	0	0	0	0	0	(
	point31	31	0	0	0	0	0	0	0	0	0	(
	point32	32	0	0	0	0	0	0	0	0	0	(
	point33	33										
Town Center drive	point34	34	1353	35	27	35	13	35	0	0	0	(
	point35	35	1353	35	27	35	13	35	0	0	0	(
	point36	36	1353	35	27	35	13	35	0	0	0	(
	point37	37	1353	35	27	35	13	35	0	0	0	(
	point38	38	1353	35	27	35	13	35	0	0	0	(
	point39	39										
Roadway5	point40	40	230	40	4	40	2	40	0	0	0	(
	point41	41	0	0	0	0	0	0	0	0	0	(
	point42	42	0	0	0	0	0	0	0	0	0	(
	point43	43	0	0	0	0	0	0	0	0	0	(
	point44	44	0	0	0	0	0	0	0	0	0	(
	point45	45	0	0	0	0	0	0	0	0	0	(
	point46	46	0	0	0	0	0	0	0	0	0	(
	point47	47										
Birch West	point48	48	1698	50	35	50	17	50	0	0	0	(
	point49	49	1698	50	35	50	17	50	0	0	0	(
	point50	50	1698	50	35	50	17	50	0	0	0	(
	point51	51	1698	50	35	50	17	50	0	0	0	(
	point52	52	1698	50	35	50	17	50	0	0	0	(
	point53	53	1698	50	35	50	17	50	0	0	0	(
	point54	54	1698	50	35	50	17	50	0	0	0	(
	point55	55										
Birch east	point56	56	1698	50	35	50	17	50	0	0	0	(
	point57	57	1698	50	35	50	17	50	0	0	0	(
	point58	58	1698	50	35	50	17	50	0	0	0 0 0 0 0 0 0 0 0 0 0	(
	point59	59	1698	50	35	50	17	50	0	0	0	(

NPUT: TRAFFIC FOR LAeq1h	Volumes					Ota	y Village	Town	Center			
•	point60	60	1698	50	35	50	17	50	0	0	0	(
	point61	61	1698	50	35	50	17	50	0	0	0	(
	point62	62	1698	50	35	50	17	50	0	0	0	(
	point63	63	1698	50	35	50	17	50	0	0	0	(
	point64	64	1698	50	35	50	17	50	0	0	0	(
	point65	65	1698	50	35	50	17	50	0	0	0	(
	point66	66										
Eastlake Pkwy	point67	67	1626	50	33	50	16	50	0	0	0	(
	point68	68	1626	50	33	50	16	50	0	0	0	(
	point69	69	1626	50	33	50	16	50	0	0	0	(
	point70	70	1626	50	33	50	16	50	0	0	0	(
	point71	71	1626	50	33	50	16	50	0	0	0	(
	point72	72	1626	50	33	50	16	50	0	0	0	(
	point73	73	1626	50	33	50	16	50	0	0	0	(
	point74	74	1626	50	33	50	16	50	0	0	0	(
	point75	75	1626	50	33	50	16	50	0	0	0	(
	point76	76										
Olympic west	point77	77	1415	50	29	50	14	50	0	0	0	(
	point78	78	1415	50	29	50	14	50	0	0	0	(
	point79	79	1415	50	29	50	14	50	0	0	0	(
	point80	80	1415	50	29	50	14	50	0	0	0	(
	point81	81	1415	50	29	50	14	50	0	0	0	(
	point82	82	1415	50	29	50	14	50	0	0	0	(
	point83	83	1415	50	29	50	14	50	0	0	0	(
	point84	84										
Olympic east	point85	85	1415	50	29	50	14	50	0	0	0	(
	point86	86	1415	50	29	50	14	50	0	0	0	(
	point87	87	1415	50	29	50	14	50	0	0	0	(
	point88	88	1415	50	29	50	14	50	0	0	0	(
	point89	89	1415	50	29	50	14	50	0	0	0	(
	point90	90	1415	50	29	50	14	50	0	0	0	(
	point91	91	1415	50	29	50	14	50	0	0	0	(
	point92	92	1415	50	29	50	14	50	0	0	0	(
	point93	93	1415	50	29	50	14	50	0	0	0	(
	point94	94	1415	50	29	50	14	50	0	0	0	(
	point95	95	1415	50	29	50	14	50	0	0	0	(

INPUT: TRAFFIC FOR LAeq1h Volumes				Ota	ay Village	<b>Town</b>	Center		
	point96	96							

INPUT: RECEIVERS								(	Otay Villa	ge Tow	n Center		
Dudek CB							August M 2.5	2022					
INPUT: RECEIVERS													
PROJECT/CONTRACT:		_	Town Center										
RUN:	Existi	ng + Pr	oject										
Receiver													
Name	No.	#DUs	Coordinates	(ground)		Hei	ight	Input Sou	nd Levels	and C	riteria		Active
			X	Υ	Z	abo	ove	Existing	Impact C	Criteria	NR		in
						Gro	ound	LAeq1h	LAeq1h	Sub'l	Goal	İ	Calc.
			ft	ft	ft	ft		dBA	dBA	dB	dB		
Town Center Dog Park	1	1	6,339,836.0	1,806,980.8	0.	00	4.92	60.90	6	66	10.0	8.0	Υ
ST1	2	1	6,339,381.0	1,807,674.9	0.	00	4.92	56.90	6	66	10.0	8.0	Υ
ST2	3	1	6,339,406.0	1,808,385.9	0.	00	4.92	55.40	6	66	10.0	8.0	Υ
B1-1-1	20	1	6,339,870.0	1,808,064.8	0.	00	4.92	0.00	6	66	10.0	8.0	Y
B1-1-2	21	1	6,339,870.0	1,808,064.8	0.	00	14.92	0.00	6	66	10.0	8.0	Y
B1-1-3	22	1	6,339,870.0	1,808,064.8	0.	00	24.92	0.00	6	66	10.0	8.0	Y
B1-1-4	23	1	6,339,870.0	1,808,064.8	0.	00	34.92	0.00	6	66	10.0	8.0	Υ
B2-1-1	24	1	6,340,266.5	1,808,159.4	0.	00	4.92	0.00	6	66	10.0	8.0	Y
B2-1-2	25	1	6,340,266.5	1,808,159.4	0.	00	14.92	0.00	6	66	10.0	8.0	
B2-1-3	26	1	6,340,266.5	1,808,159.4	0.	00	24.92	0.00	6	66	10.0	8.0	
B2-1-4	27	1	6,340,266.5	1,808,159.4	0.	00	34.92	0.00	6	66	10.0	8.0	
B3-1-1	28	1	6,340,121.0	1,807,750.9	0.	00	4.92	0.00	6	66	10.0	8.0	
B3-1-2	30	1	6,340,121.0	1,807,750.9	0.	00	14.92		6	66	10.0	8.0	
B3-1-3	31	1	6,340,121.0	1,807,750.9	0.	00	24.92		6	66	10.0	8.0	
B3-1-4	33	1	6,340,121.0	1,807,750.9	0.	00	34.92	0.00	6	66	10.0	8.0	
B1-2-1	34		-,,-			00	4.92			66	10.0	8.0	
B1-2-2	35		<u> </u>			00	14.92			66	10.0	8.0	
B1-2-3	36		-,,			00	24.92			66	10.0	8.0	
B1-2-4	37		6,339,743.0	1,807,905.1		00	34.92			66	10.0	8.0	
B3-2-1	38		-,,	1 1		00	4.92			66	10.0	8.0	
B3-2-2	39		-,,-	1		00	14.92			66	10.0	8.0	
B3-2-3	40	1	6,339,925.5	1,807,559.1	0.	00	24.92	0.00	6	66	10.0	8.0	Y

INPUT: RECEIVERS Otay Village Town Center

B3-2-4	41	1	6,339,925.5	1,807,559.1	0.00	34.92	0.00	66	10.0	8.0	Υ
B3-3-1	42	1	6,340,127.0	1,807,440.9	0.00	4.92	0.00	66	10.0	8.0	Υ
B3-3-2	43	1	6,340,127.0	1,807,440.9	0.00	14.92	0.00	66	10.0	8.0	Υ
B3-3-3	44	1	6,340,127.0	1,807,440.9	0.00	24.92	0.00	66	10.0	8.0	Υ
B3-3-4	46	1	6,340,127.0	1,807,440.9	0.00	34.92	0.00	66	10.0	8.0	Υ
OS-1	48	1	6,340,091.5	1,807,993.8	0.00	4.92	0.00	66	10.0	8.0	Υ

Dudek					26 Augi	ust 2022	2											
СВ					TNM 2.5	5												
INPUT: BARRIERS																		
PROJECT/CONTRACT:	Otay	Village T	own Cer	nter														
RUN:	Existi	ing + Pro	ject															
Barrier									Points									
Name	Туре	Height		If Wall	If Berm			Add'tnl	Name	No.	Coordinates	(bottom)		Height	Segment			
		Min	Max	\$ per	\$ per	Тор	Run:Rise	\$ per			x	Υ	Z	at	Seg Ht Per	turbs	On	Importan
				Unit	Unit	Width		Unit						Point	Incre- #Up	#Dn	Struct?	Reflec-
				Area	Vol.			Length							ment			tions?
		ft	ft	\$/sq ft	\$/cu yd	ft	ft:ft	\$/ft			ft	ft	ft	ft	ft			
Barrier1	W	0.00	99.99	0.00				0.00	point1	1	6,339,727.0	1,808,050.1	0.00	40.00	0.00	0 (	)	
									point2	2	6,339,763.0	1,807,788.5	0.00	40.00	0.00	0 (	כ	
									point3	3	6,340,071.5	1,807,828.0	0.00	40.00	0.00	0 (	)	
									point4	4	6,340,042.0	1,808,077.9	0.00	40.00	0.00	0 (	)	
									point5	5	6,339,852.5	1,808,057.1	0.00	40.00	0.00	0 (	)	
									point6	6	6,339,852.5	1,808,066.1	0.00	40.00	0.00	0 (	)	
									point7	7	6,339,727.0	1,808,050.1	0.00	40.00				
Barrier2	W	0.00	99.99	0.00				0.00	point8	8		1,807,836.6	0.00	40.00	0.00	0 (	)	
									point9	9	6,340,514.0	1,807,881.5	0.00	40.00	0.00	0 (	)	
									point10	10	-,,	1,807,966.0			0.00	0 (	ס	
									point11	11	-,,	1,807,966.5				0 (	)	
									point12	12		1,807,990.9				0 (	ס	
									point13	13		1,807,992.1	0.00			-	)	
									point14	14	-,,	1,808,201.2					)	
									point15		6,340,112.5	1,808,113.8				0 (	)	
									point16		6,340,147.5	1,807,836.6						
Barrier3	W	0.00	99.99	0.00				0.00	•	17	-,,	1,807,715.4				-	)	
									point18	18	-,,-	1,807,421.2					)	
									point19	19	-,,	1,807,476.6				-	)	
									point20	20	-,,	1,807,770.9			0.00	0 (	)	
									point21	21	6,339,906.5	1,807,715.4	0.00	40.00				

## **INPUT: TERRAIN LINES**

Dudek			26 August 20	22
СВ			TNM 2.5	
INPUT: TERRAIN LINES				
PROJECT/CONTRACT:	Otay V	illage Town C	enter	
RUN:	Existin	g + Project		
Terrain Line Name	Points			
	No.	Coordinates	(ground)	
		X	Υ	Z
		ft	ft	ft
Terrain Line1	1	6,339,688.0	1,807,583.2	0.00
	2	6,339,667.5	1,807,799.5	0.00
	3	6,339,644.0	1,807,921.2	0.00
	4	6,339,647.5	1,808,134.1	0.00
	5	6,339,654.0	1,808,178.0	0.00

		1											
Dudeli							00 4						
Dudek							26 August	1 2022					
СВ							TNM 2.5	al:41a TNII					
							Calculate	a with I Ni	WI 2.5		1		
RESULTS: SOUND LEVELS													
PROJECT/CONTRACT:		_	Ilage Town										
RUN:			g + Project								<u> </u>		
BARRIER DESIGN:		INPUT	HEIGHTS					_	pavement type ighway agenc			e	
ATMOSPHERICS:		68 deg	F, 50% RH	1				of a diffe	rent type with	approval of F	HWA.		
Receiver													
Name	No.	#DUs	Existing	No Barrier					With Barrier				
			LAeq1h	LAeq1h	-	Increase over	existing	Туре	Calculated	Noise Reduc	tion		
				Calculated	Crit'n	Calculated	Crit'n	Impact	LAeq1h	Calculated	Goal	Calculat	ted
							Sub'l Inc					minus	
												Goal	
			dBA	dBA	dBA	dB	dB		dBA	dB	dB	dB	
Town Center Dog Park	1	1	60.9	60.0	) 66	-0.9	9 10		60.0	0.0		8	-8.0
ST1	2	. 1	56.9	68.2	2 66	11.3	3 10	Both	68.2	0.0		8	-8.0
ST2	3	1	55.4	68.8	3 66	3 13.4	4 1C	Both	68.8	0.0		8	-8.0
B1-1-1	20	1	0.0	54.0	66	54.6	3 10		54.6	0.0		8	-8.0
B1-1-2	21	1	0.0	58.4	4 66	58.4	4 1C		58.4	0.0		8	-8.0
B1-1-3	22	! 1	0.0	60.0	) 66	60.0	) 10		60.0	0.0		8	-8.0
B1-1-4	23	1	0.0	60.3	3 66	60.3	3 10		60.3	0.0		8	-8.0
B2-1-1	24	. 1	0.0	51.	3 66	51.3	3 10		51.3	0.0		8	-8.0
B2-1-2	25	1	0.0	55.0	66	55.6	3 10		55.6	0.0		8	-8.0
B2-1-3	26	1	0.0	57.	7 66	57.7	7 10		57.7	0.0		8	-8.0
B2-1-4	27		0.0	58.			1 10		58.1	0.0		8	-8.0
B3-1-1	28		0.0	40.4	4 66	6 40.4	4 1C		40.4	0.0		8	-8.0
B3-1-2	30	1	0.0	) 44.:	2 66	44.2	2 10		44.2	0.0		8	-8.0
B3-1-3	31	1	0.0	46.	1 66	46.1	1 10		46.1	0.0		8	-8.0
B3-1-4	33		0.0	47.9					47.9	0.0		8	-8.0
B1-2-1	34		0.0	58.3					58.3	0.0		8	-8.0
B1-2-2	35								63.7			8	-8.0
B1-2-3	36								65.0			8	-8.0
B1-2-4	37								65.8			8	-8.0
B3-2-1	38								51.6			8	-8.0
B3-2-2	39								55.5			8	-8.0
B3-2-3	40								59.5			8	-8.0
B3-2-4	41								60.2			8	-8.0
B3-3-1	42	! 1	0.0	51.9	9 66	51.9	9 10		51.9	0.0		8	-8.0

## **RESULTS: SOUND LEVELS**

B3-3-2	43	1		0.0	54.9	6	6	54.9	10	 54.9	0.0	8	-8.0
B3-3-3	44	1		0.0	56.9	6	6	56.9	10	 56.9	0.0	8	-8.0
B3-3-4	46	1		0.0	57.8	6	6	57.8	10	 57.8	0.0	8	-8.0
OS-1	48	1		0.0	39.7	6	6	39.7	10	 39.7	0.0	8	-8.0
Dwelling Units		# DUs	Noise	Reduction									
			Min	Avg		Max							
			dB	dB		dB							
All Selected		28		0.0	0.0	0.	0						
All Impacted		2		0.0	0.0	0.	0						
All that meet NR Goal		0		0.0	0.0	0.	0						

noise level limit for construction phase at residential land use, per FTA guidance = allowable hours over which Leq is to be averaged =

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq
Demolition	Concrete saw	1	20	90	Concrete/Industrial Saws	325	0.1		69.2	8	480	62
	Dozer	1	40	82		325	0.1		61.2	8	480	57
	front end loader	2	40	79		325	0.1		58.2	8	480	57
	excavator	2	40	81		325	0.1		60.2	8	480	59
			_	•		-	_		Total for De	emolition Phase:		65.5
Site Preparation	Dozer	2	40	82		330	0.1		61.0	8	480	60
	Tractor	1	40	84		330	0.1		63.0	8	480	59
	front end loader	1	40	79		330	0.1		58.0	8	480	54
	Backhoe	0	40	78		330	0.1		57.0	8	480	0
			_	•		-	_		Total for Site Pre	paration Phase:		63.2
Underground Utilities	Tractor	1	40	84		340	0.1		62.7	8	480	59
	front end loader	1	40	79		340	0.1		57.7	8	480	54
	Backhoe	0	40	78		340	0.1		56.7	8	480	0
			_			-	<u>-</u>	Tota	I for Underground	Utilities Phase:		59.9
Grading	excavator	1	40	81		330	0.1		60.0	8	480	56
	grader	1	40	85		330	0.1		64.0	8	480	60
	dozer	1	40	82		330	0.1		61.0	8	480	57
	tractor	1	40	84		330	0.1		63.0	8	480	59
	front end loader	1	40	79		330	0.1		58.0	8	480	54
	backhoe	0	40	78		330	0.1		57.0	8	480	0
			-	·		-	_		Total for	Grading Phase:		64.7
Building Construction	crane	1	16	81		340	0.1		59.7	7	420	51
	man lift	2	20	75	forklift	340	0.1		53.7	8	480	50
	generator	1	50	72		340	0.1		50.7	8	480	48
	tractor	1	40	84		340	0.1		62.7	7	420	58
	front end loader	1	40	79		340	0.1		57.7	7	420	53
	backhoe	1	40	78		340	0.1		56.7	7	420	52
	welder / torch	1	40	73		340	0.1		51.7	4	240	45
								Tota	for Building Con	struction Phase:		61.3
Paving	Concrete mixer truck	2	40	79	Cement and Mortar Mixers	450	0.1		55.0	6	360	53
	paver	1	50	77		450	0.1		53.0	8	480	50
	All Other Equipment > 5 HP	2	50	85	Paving Equipment	450	0.1		61.0	6	360	60
	roller	2	20	80		450	0.1		56.0	6	360	51
	tractor	1	40	84		450	0.1		60.0	8	480	56
	front end loader	0	40	79		450	0.1		55.0	8	480	0
	backhoe	0	40	78		450	0.1		54.0	8	480	0
		•	•	'		-			Total fo	r Paving Phase:		62.5
Architectural Coating	compressor (air)	1	40	78		340	0.1		56.7	6	360	52
•		· ·	-	'		-		Tota	ı I for Architectural	Coating Phase:		51.5

noise level limit for construction phase at residential land use, per FTA guidance = allowable hours over which Leq is to be averaged =

**80** 

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq
Demolition	Concrete saw	1	20	90	Concrete/Industrial Saws	555	0.1		64.0	8	480	57
	Dozer	1	40	82		555	0.1		56.0	8	480	52
	front end loader	2	40	79		555	0.1		53.0	8	480	52
	excavator	2	40	81		555	0.1		55.0	8	480	54
			_			_			Total for De	molition Phase:		60.3
Site Preparation	Dozer	2	40	82		510			56.8	8	480	56
	Tractor	1	40	84		510	0.1		58.8	8	480	55
	front end loader	1	40	79		510	0.1		53.8	8	480	50
	Backhoe	0	40	78		510	0.1		52.8	8	480	0
			_			_	_		Total for Site Prep	paration Phase:		59.0
Underground Utilities	Tractor	1	40	84		505	0.1		58.9	8	480	55
	front end loader	1	40	79		505			53.9	8	480	50
	Backhoe	0	40	78		505	0.1		52.9	8	480	0
			_			_		Tota	I for Underground	Utilities Phase:		56.1
Grading	excavator	1	40	81		510	0.1		55.8	8	480	52
	grader	1	40	85		510	0.1		59.8	8	480	56
	dozer	1	40	82		510	0.1		56.8	8	480	53
	tractor	1	40	84		510	0.1		58.8	8	480	55
	front end loader	1	40	79		510	0.1		53.8	8	480	50
	backhoe	0	40	78		510	0.1		52.8	8	480	0
			_			_	_		Total for	Grading Phase:		60.5
Building Construction	crane	1	16			505	0.1		55.9	7	420	47
	man lift	2	20	75	forklift	505			49.9	8	480	46
	generator	1	50	72		505			46.9	8	480	44
	tractor	1	40	84		505			58.9	7	420	54
	front end loader	1	40	79		505			53.9	7	420	49
	backhoe	1	40	78		505			52.9	7	420	48
	welder / torch	1	40	73		505	0.1		47.9	4	240	41
			_			_		Tota	I for Building Cons	truction Phase:		57.5
Paving	Concrete mixer truck	2	40	79	Cement and Mortar Mixers	460	0.1		54.8	6	360	53
	paver	1	50	77		460	0.1		52.8	8	480	50
	All Other Equipment > 5 HP	2	50	85	Paving Equipment	460	0.1		60.8	6	360	60
	roller	2	20	80		460	0.1		55.8	6	360	51
	tractor	1	40	84		460	0.1		59.8	8	480	56
	front end loader	0	40	79		460	0.1		54.8	8	480	0
	backhoe	0	40	78		460	0.1		53.8	8	480	0
		-	•			_			Total for	Paving Phase:		62.3
Architectural Coating	compressor (air)	1	40	78		505	0.1		52.9	6	360	48
-		•	-			-		Tota	al for Architectural	Coating Phase:		47.7

noise level limit for construction phase at residential land use, per FTA guidance = allowable hours over which Leq is to be averaged =

80 8

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq
Demolition	Concrete saw	1	20	90	Concrete/Industrial Saws	705	0.1		61.7	8	480	55
	Dozer	1	40	82		705	0.1		53.7	8	480	50
	front end loader	2	40	79		705	0.1		50.7	8	480	50
	excavator	2	40	81		705	0.1		52.7	8	480	52
	·		_			_			Total for De	molition Phase:		58.0
Site Preparation	Dozer	2	40	82		700	0.1		53.8	8	480	53
	Tractor	1	40	84		700	0.1		55.8	8	480	52
	front end loader	1	40	79		700	0.1		50.8	8	480	47
	Backhoe	0	40	78		700	0.1		49.8	8	480	0
			_			_	_		Total for Site Preg	aration Phase:		55.9
Underground Utilities	Tractor	1	40	84		710	0.1		55.6	8	480	52
	front end loader	1	40	79		710			50.6	8	480	47
	Backhoe	0	40	78		710	0.1		49.6	8	480	0
			_					Tota	for Underground	Utilities Phase:		52.9
Grading	excavator	1	40	81		700			52.8	8	480	49
	grader	1	40	85		700	0.1		56.8	8	480	53
	dozer	1	40	82		700			53.8	8	480	50
	tractor	1	40	84		700	0.1		55.8	8	480	52
	front end loader	1	40	79		700			50.8	8	480	47
	backhoe	0	40	78		700	0.1		49.8	8	480	0
			_						Total for 0	Grading Phase:		57.5
Building Construction	crane	1	16			710	0.1		52.6	7	420	44
	man lift	2	20	75	forklift	710			46.6	8	480	43
	generator	1	50			710	0.1		43.6	8	480	41
	tractor	1	40	84		710	0.1		55.6	7	420	51
	front end loader	1	40	79		710			50.6	7	420	46
	backhoe	1	40	78		710	0.1		49.6	7	420	45
	welder / torch	1	40	73		710	0.1		44.6	4	240	38
								Tota	I for Building Cons	truction Phase:		54.2
Paving	Concrete mixer truck	2	40	79	Cement and Mortar Mixers	860	0.1		48.8	6	360	47
	paver	1	50	77		860	0.1		46.8	8	480	44
	All Other Equipment > 5 HP	2	50	85	Paving Equipment	860	0.1		54.8	6	360	54
	roller	2	20	80		860	0.1		49.8	6	360	45
	tractor	1	40	84		860	0.1		53.8	8	480	50
	front end loader	0	40	79		860	0.1		48.8	8	480	0
	backhoe	0	40	78		860	0.1		47.8	8	480	0
			_			_	•		Total for	Paving Phase:		56.2
Architectural Coating	compressor (air)	1	40	78		710	0.1		49.6	6	360	44
-	• • • • •	•	-			-		Tota	I for Architectural	Coating Phase:		44.4

noise level limit for construction phase at re

residential land use, per FTA guidance =	80
ours over which Leq is to be averaged =	8

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq
Demolition	Concrete saw	1	20	90	Concrete/Industrial Saws	1050	0.1		57.8	8	480	51
	Dozer	1	40	82		1050	0.1		49.8	8	480	46
	front end loader	2	40	79		1050	0.1		46.8	8	480	46
	excavator	2	40	81		1050	0.1		48.8	8	480	48
			-			_				molition Phase:		54.1
Site Preparation	Dozer	2	40	82		920			51.1	8	480	50
	Tractor	1	40	84		920			53.1	8	Section   Continue	49
	front end loader	1	40	79		920			48.1	8	480	44
	Backhoe	0	40	78		920	0.1		47.1	8	480	0
			_			_			Total for Site Pre	paration Phase:		53.2
Underground Utilities	Tractor	1	40	84		900			53.3	8	480	49
	front end loader	1	40	79		900			48.3	8	480	44
	Backhoe	0	40	78		900	0.1		47.3	8	480	0
			_			_		Tota	for Underground	Utilities Phase:		50.5
Grading	excavator	1	40	81		920	0.1		50.1	8	480	46
	grader	1	40	85		920	0.1		54.1	8	480	50
	dozer	1	40	82		920	0.1		51.1	8	480	47
	tractor	1	40	84		920	0.1		53.1	8	480	49
	front end loader	1	40	79		920	0.1		48.1	8	ase:	44
	backhoe	0	40	78		920	0.1		47.1	8	480	0
			_			_			Total for	Grading Phase:		54.8
Building Construction	crane	1	16	81		900	0.1		50.3	7	420	42
	man lift	2	20	75	forklift	900	0.1		44.3	8	480	40
	generator	1	50	72		900	0.1		41.3	8	480	38
	tractor	1	40	84		900	0.1		53.3	7	420	49
	front end loader	1	40	79		900	0.1		48.3	7	420	44
	backhoe	1	40	78		900	0.1		47.3	7	420	43
	welder / torch	1	40	73		900	0.1		42.3	4	240	35
						_		Total	for Building Con	struction Phase:		51.9
Paving	Concrete mixer truck	2	40	79	Cement and Mortar Mixers	870	0.1		48.7	6	360	46
	paver	1	50	77		870	0.1		46.7	8	Sec.   Sec.	44
	All Other Equipment > 5 HP	2	50	85	Paving Equipment	870	0.1		54.7	6		53
	roller	2	20	80		870	0.1		49.7	6	360	44
	tractor	1	40	84		870	0.1		53.7	8	480	50
	front end loader	0	40	79		870	0.1		48.7	8	480	0
	backhoe	0	40	78		870	0.1		47.7	8	480	0
	-		-			_			Total fo	r Paving Phase:		56.1
Architectural Coating	compressor (air)	1	40	78		900	0.1		47.3	6	360	42
			-			-		Tota	I for Architectural	Coating Phase:		42.1

noise level limit for construction phase at residential land use, per FTA guidance = allowable hours over which Leq is to be averaged =

uidance = 8

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq
Demolition	Concrete saw	1	20	90	Concrete/Industrial Saws	330	0.1		69.0	8	480	62
	Dozer	1	40	82		330	0.1		61.0	8	480	57
	front end loader	2	40	79		330	0.1		58.0	8	480	57
	excavator	2	40	81		330	0.1		60.0	8	480	59
	•		_			_			Total for De	molition Phase:		65.3
Site Preparation	Dozer	2	40	82		320	0.1		61.3	8	480	60
	Tractor	1	40	84		320	0.1		63.3	8	480	59
	front end loader	1	40	79		320	0.1		58.3	8	480	54
	Backhoe	0	40	78		320	0.1		57.3	8	480	0
			_			_			Total for Site Prep	aration Phase:		63.5
Underground Utilities	Tractor	1	40	84		520	0.1		58.6	8	480	55
	front end loader	1	40	79		520	0.1		53.6	8	480	50
	Backhoe	0	40	78		520	0.1		52.6	8	480	0
			_			_		Tota	l for Underground	Utilities Phase:		55.9
Grading	excavator	1	40	81		320	0.1		60.3	8	480	56
	grader	1	40	85		320	0.1		64.3	8	480	60
	dozer	1	40	82		320	0.1		61.3	8	480	57
	tractor	1	40	84		320	0.1		63.3	8	480	59
	front end loader	1	40	79		320	0.1		58.3	8	480	54
	backhoe	0	40	78		320	0.1		57.3	8	480	0
	•	-	_			_			Total for (	Grading Phase:		65.0
Building Construction	crane	1	16	81		520	0.1		55.6	7	420	47
	man lift	2	20	75	forklift	520	0.1		49.6	8	480	46
	generator	1	50	72		520	0.1		46.6	8	480	44
	tractor	1	40	84		520	0.1		58.6	7	420	54
	front end loader	1	40	79		520	0.1		53.6	7	420	49
	backhoe	1	40	78		520	0.1		52.6	7	420	48
	welder / torch	1	40	73		520	0.1		47.6	4	240	41
		•	-			-		Tota	I for Building Cons	truction Phase:		57.2
Paving	Concrete mixer truck	2	40	79	Cement and Mortar Mixers	440	0.1		55.2	6	360	53
	paver	1	50	77		440	0.1		53.2	8	480	50
	All Other Equipment > 5 HP	2	50	85	Paving Equipment	440	0.1		61.2	6	360	60
	roller	2	20	80		440	0.1		56.2	6	360	51
	tractor	1	40	84		440	0.1		60.2	8	480	56
	front end loader	0	40			440			55.2	8	480	0
	backhoe	0	40			440			54.2	8	480	0
										Paving Phase:		62.7
Architectural Coating	compressor (air)	1	40	78		520	0.1		1 52.6 <b>[</b>	6	360	47
	Tamprooon (all)	<del></del>	1	70		1 020	V.1	Tele	I for Architectural		300	47.4

noise level limit for construction phase at residential land use, per FTA guidance = allowable hours over which Leq is to be averaged =

dance = 8 raged =

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq
Demolition	Concrete saw	1	20	90	Concrete/Industrial Saws	750	0.1		61.1	8	480	
	Dozer	1	40	82		750	0.1		53.1	8	480	
	front end loader	2	40	79		750	0.1		50.1	8	480	
	excavator	2	40	81		750	0.1		52.1	8	480	
			_			_			Total for De	emolition Phase:		5
ite Preparation	Dozer	2	40	82		775	0.1		52.8	8	480	
front end loader         2         40         79           excavator         2         40         81		775	0.1		54.8	8	480					
	front end loader	1	40	79		775	0.1		49.8	8	8 8 480 480 88 480 480 88 480 480 88 480 480	
	Backhoe	0	40	78		775	0.1		48.8	8	480	
			_			_			Total for Site Pre	paration Phase:		
nderground Utilities	Tractor	1	40	84		785	0.1		54.7	8	480	
	front end loader	1	40	79		785	0.1		49.7	8	B	
	Backhoe	0	40	78		785	0.1		48.7	8	480	
			_					Tota	for Underground	Utilities Phase:		
Grading	excavator	1	40	81		775	0.1		51.8	8	480	
	grader	1	40	85		775	0.1		55.8	8	480	
	dozer	1	40	82		775	0.1		52.8	8		
	tractor	1	40	84		775	0.1		54.8	8	480	
	front end loader	1	40	79		775	0.1		49.8	8	480	
	backhoe	0	40	78		775	0.1		48.8	8	480	
			_			_			Total for	Grading Phase:		
uilding Construction	crane	1	16	81		785	0.1		51.7	7	420	
	man lift	2	20	75	forklift	785	0.1		45.7	8	480	
	generator	1	50	72		785	0.1		42.7	8	480	
	tractor	1	40	84		785	0.1		54.7	7	420	
	front end loader	1	40	79		785	0.1		49.7	7	420	
	backhoe	1	40	78		785	0.1		48.7	7	420	
	welder / torch	1	40	73		785	0.1		43.7	4	240	
	•	-	=			_	_	Tota	for Building Con	struction Phase:		
aving	Concrete mixer truck	2	40	79	Cement and Mortar Mixers	730	0.1		50.4	6	360	
	paver	1	50	77		730	0.1		48.4	8	Operation Time (minutes)  480 480 480 480 480 480 480 480 480 48	
	All Other Equipment > 5 HP	2	50	85	Paving Equipment	730	0.1		56.4	6	360	
	roller	2	20	80		730	0.1		51.4	6	360	
	tractor	1	40	84		730	0.1		55.4	8	480	
	front end loader	0	40	79		730	0.1		50.4	8	480	
	backhoe	0	40	78		730	0.1		49.4	8	480	
			•			_			Total fo	r Paving Phase:	480 480 480 480 480 480 480 480 480 480	
rchitectural Coating	compressor (air)	1	1 40	78		785	0.1		48.7	6	360	